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THE EFFECT OF WEATHERING ON OCTANE QUALITY FOR
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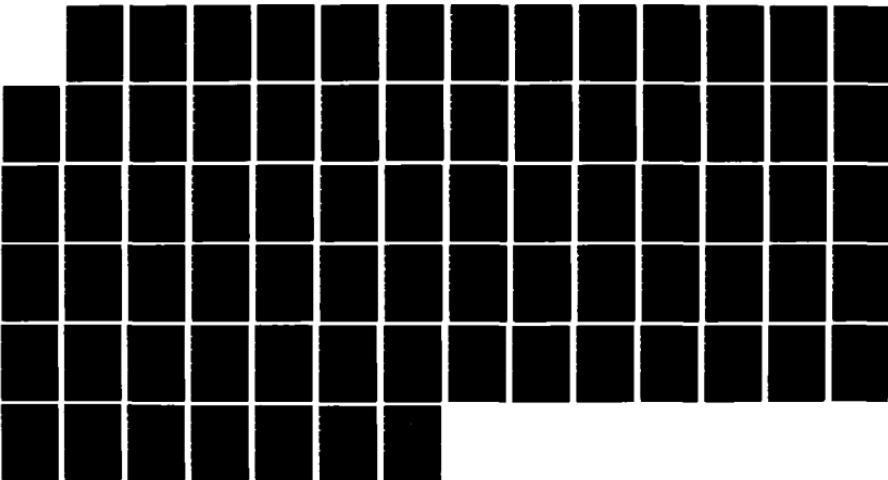
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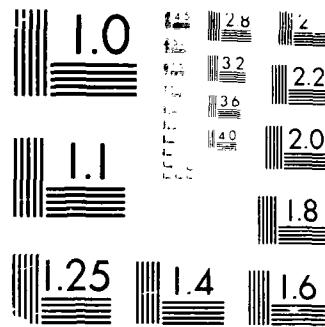
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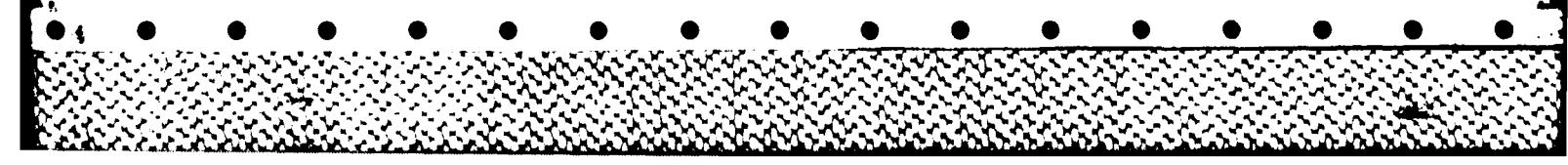
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The Effect of Weathering on Octane Quality for Winter-Grade and Summer-Grade Gasolines

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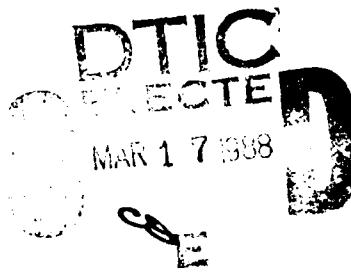
December 1987

Final Report

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Technical Report Documentation Page

1. Report No. DOT/FAA/CT-87/16	2. Government Accession No. ADA190640	3. Recipient's Catalog No.
4. Title and Subtitle The Effect of Weathering on Octane Quality for Winter-Grade and Summer-Grade Gasolines		5. Report Date December 1987
7. Author(s) Richard N. Wares		6. Performing Organization Code
9. Performing Organization Name and Address National Institute for Petroleum and Energy Research (NIPER) P.O. Box 2128, Bartlesville, OK 74005		8. Performing Organization Report No.
12. Sponsoring Agency Name and Address U.S. Department of Transportation Federal Aviation Administration Technical Center Atlantic City Airport, New Jersey 08405		10. Work Unit No. (TRAIS)
15. Supplemental Notes		11. Contract or Grant No. Coop Agrmt DE-FC22-83FE60149
16. Abstract Weathering tests were conducted to examine the effects on fuel volatility and octane characteristics. The commercially available gasolines utilized in the study represented a wide geographic distribution for both winter and summer fuels. Aging was accomplished by heating the fuel samples to 110 degrees F and maintaining that temperature for 48 hours. Time histories of Reid Vapor Pressure (RVP) were conducted. Fuel octane evaluations, both MON and RON, were done. Component characterization by gas chromatography were made to identify components lost during the aging process. The time histories of vapor pressure changes depended to a limited measure on the initial fuel vapor pressure as well as to differences in composition. Butanes and isopentanes were the primary constituents lost due to the weathering. For the most part octane changes due to fuel weathering were minimal.		13. Type of Report and Period Covered Final Report
17. Key Words Volatility Changes Octane Changes Alkene Gas Chromatography Automobile Gasoline Oxidation		18. Distribution Statement This document is available to the U.S. public through the National Technical Information Service, Springfield, Virginia 22161
19. Security Classif. (of this report)	20. Security Classif. (of this page)	21. No. of Pages
		22. Price

ACKNOWLEDGMENT

The work described in this report was performed in partial fulfillment of the requirements of the Cooperative Agreement DE-FC22-83FF60149 between the U.S. Department of Energy and the IIT Research Institute with primary sponsorship by the Federal Aviation Administration. In particular, the efforts of Mr. Gus Ferrara who provided direction for the FAA and assistance in the effort is acknowledged. Mr. Alex Crawley of the Bartlesville Project Office in Bartlesville, Oklahoma, coordinated the effort for the U.S. Department of Energy.

Approved by:	
NTIS Serial:	X
FDIC ID:	
Unnumbered:	
Justification:	
By:	
Distribution:	
Finality Dates:	
Comments:	
Dist. Specifi:	
A-1	



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EXECUTIVE SUMMARY

This report describes studies conducted at the National Institute of Petroleum and Energy Research (NIPER) for the Federal Aviation Administration (FAA) under a cost sharing agreement with the U.S. Department of Energy. In these studies, the effect of aging automobile gasoline on its volatility and its octane rating was measured.

The samples tested in this program represented a wide geographic distribution for both winter and summer blends of automobile gasoline. Aging was accomplished by heating the samples to 110° F in vented containers and keeping the fuel sample at that temperature for 48 hours. The change in the volatility of the fuel was measured using the Reid Vapor Pressure (or an equivalent test and correcting it to the Reid Vapor Pressure). The research and motor octane numbers were measured before and after aging. The distillation curve of each fuel was determined for both the initial and aged samples. The constituents of each fuel were identified for both the initial and aged samples using gas chromatography and the principle constituents lost during aging were identified.

The changes in the distillation curve and the Reid Vapor Pressure were greater for the winter-grade fuels than the summer-grade fuels. This was expected since the winter-grade fuels contain a larger percentage of low molecular weight constituents (e.g., butane and isopentane) and these are the principle components lost during the aging process.

The changes in octane as a consequence of aging were, for the most part, negligible. The principle exception was for the winter-grade sample of fuel from Philadelphia which contained an unusually high percentage of butane. The change in octane rating was similar for both the winter grade and the summer grade fuels.

WEATHERING EFFECTS ON FUEL QUALITY

INTRODUCTION

The mandated reduction in fuel lead level and an increasing demand for high octane quality fuels necessary for maximum performance of vehicles require refineries to consider all possible means to produce acceptable quality fuels at competitive costs.

In the light aircraft industry, concerns exist that the substitution of motor gasoline for aviation gasoline might result in engine failure during maximum power demands. Weathered fuels which have lost higher volatility components will have qualities that are more closely related to the remaining lower volatility components. The bulk of the remaining portion lies in the distillation range that would be produced from alternative feedstocks and these tend to be the lower octane components. Requests to the Federal Aviation Administration (FAA) for autogas certification have raised questions concerning current regulations. The fuel certification procedures require aircraft fuel tests to be conducted at 110° F. Concerns are related to the higher volatility characteristics of autogas compared to aviation gas and the possibility of inducing vapor lock at high temperatures. There is also inadequate information regarding the weathering effect of fuel storage at high temperature and resultant effects on fuel octane quality.

EXPERIMENTAL PROGRAM

The experimental program at the National Institute for Petroleum and Energy Research (NIPER) was initiated to provide information to aid in making technical judgments on fuel, fuel specifications, and fuel conditioning requirements for a range of fuels that could be utilized in current light aircraft. This portion of the work is centered on determining the acceptability of motor fuels that have been weathered, causing loss of volatile components.

TEST FUELS.

Commercial auto gasolines from various locations were surveyed for volatility and octane quality--in both as-received and after-weathering conditions. Antiknock quality was evaluated to assess the suitability of this variety of auto fuels for aviation applications. Experiments have been conducted with ten winter (January-February) and ten summer (July-August) fuels that were obtained from commercial suppliers representing various geographic (refining) areas in the contiguous 48 states. The fuels were tested in as-received condition with no modifications to the existing vapor pressures. Specific fuel properties will be presented in the section dealing with test results.

TEST PROCEDURES.

Prior to testing, all fuels were stored in air tight sealed drums at 50° F and equilibrated at that temperature for a minimum of one week. The fuel weathering tests involved transferring the fuels to vented test tanks, heating

the fuel to 110° F and maintaining that fuel temperature for a 48-hour period. This time period was chosen to ensure noticeable aging effects following equilibration at 110° F. Fuel samples were taken within one hour of the time required for the fuel to equilibrate at 110° F and at 12, 24, and 48 hours afterward for determination of vapor pressures. In addition, fuel samples were taken both from the initial or fresh fuel and at the 48-hour point following temperature equilibration. These samples were analyzed for distillation characteristics (ASTM D 86), research octane number (RON) (ASTM D2699) and motor octane number (MON) (ASTM D2700). An attempt to identify specific components of the gasolines which are lost due to weathering at this temperature was conducted using gas chromatographic techniques.

Two fuel tanks representative of light aircraft were used. These were rectangular shaped with low height and large bottom surfaces. The total tank volumes were nominally 13 gallons. Each tank was vented through fill ports and this area was less than 2 percent of the tank top area. The tanks were placed on stands in a test cell having a temperature control range of 50° to 120° F \pm 1°. Thermocouples were placed in the tanks approximately one inch above the bottom surface to monitor fuel temperature, and additional monitoring for temperature history was made with a chart recorder. The tank levels specified were a minimum of 90 percent full.

The test procedure consists of the following:

1. Fuels were stored at an ambient temperature 50° F and an initial (fresh fuel) sample was taken under these conditions.
2. Test fuel tanks were filled with 50° F fuel to the 12-gallon (92 percent full) level.
3. Tank vents were left open to the atmosphere.
4. The tanks were then placed in the soak area and heated to a fuel temperature of 110° F. This fuel temperature was controlled by room ambient temperature throughout the test to \pm 1° F.
5. Fuel samples were taken within one hour of attaining the desired temperature. This was referred to as time = 0.
6. Additional samples were taken at 12, 24, and 48 hours following equilibration at 110° F.

As mentioned earlier, additional measurements were made with the initial and 48-hour samples. These included:

1. Distillation characteristics by ASTM D 86 technique.
2. Fuel octane evaluations--both RON and MON.
3. Component characterization by gas chromatographic analyses.

Vapor pressure measurements were made from all samples taken. The fuel samples for vapor pressure analyses were stored and equilibrated at 50° F. Vapor pressure measurements for the ten winter grade fuels were made at NIPER using the ASTM microvapor pressure (MVP) procedure D 2551-71. The MVP was measured with a model "F" vapor pressure gauge from Manufacturers Engineering and Equipment Corporation.

The micro method was developed as an alternative to the standard RVP procedure ASTM D 323 to offer an advantage in speed and size of sample required. The RVP method consisted of filling a gasoline chamber of vapor pressure apparatus with a chilled sample of gasoline. The gasoline chamber was connected to an air chamber maintained at 100° F, and the apparatus was immersed in a bath at 100° F and shaken periodically until a constant pressure was observed on a gauge attached to the apparatus. The gauge reading, suitably corrected, was reported as Reid vapor pressure.

The microvapor pressure consisted of introducing a liquid sample into an evacuated chamber fitted with means of measuring pressure in the chamber before and after sample introduction. The apparatus was immersed in a constant temperature bath of 100° F. Both the RVP and MVP procedures used vapor/liquid volume ratios of about 4:1.

When a sample of volatile hydrocarbons is saturated with air and introduced into a chamber and allowed to equilibrate, the increase in pressure is equal to the sum of the following four pressures:

1. The vapor pressure of the liquid at the temperature of the chamber.
2. The partial pressure of the dissolved air that comes out of solution.
3. The partial pressure of the dissolved water.
4. The compression effect of the liquid volume on initial air within the chamber.

The only significant pressures of these four which contribute to the total pressure are the first two, the vapor pressure of the sample and partial pressure of the dissolved air.

By nature of the systems, the evacuated chamber associated with the MVP presumes that all dissolved air will come entirely out of the solution and be measured and corrected; whereas, the Reid method (above atmospheric pressure) automatically compensates for the effect of dissolved air. Therefore, the RVP of a given sample will always be lower than the MVP of the same sample. For conversion of MVP results to RVP, the MVP may be corrected for the effect of dissolved air or empirically correlated with Reid values.

The samples were saturated with air at 50° F and pressures measured by mercury manometer at 100° F by mercury manometer. The empirical mathematical relationship of MVP and RVP was supplied with the test apparatus.

The equation:

$$ERVP, \text{ psi} = 0.01^o (\text{MVP, mmHg}) - 0.66$$

allows the measured MVP to be expressed as an equivalent Reid vapor pressure (ERVP).

The summer fuel vapor pressure measurements were made using the Reid procedure. A Herzog semi-automatic Reid vapor pressure apparatus was used. The change in vapor pressure apparatus for the summer measurements was made primarily for purpose of faster turnaround. Results from the two types of vapor pressure measurements were examined at NIFER for a variety of fuels in the pressure range of interest and were found to be very comparable.

RESULTS

WINTER-GRADE FUELS.

Table I shows a tabular history of the fuel vapor pressure changes due to weathering effects at 110° F. The fuels are identified by the city of origin. These data are presented as ERVP. The vapor pressure samples were taken within the previously defined time limits. As a group, the original or unweathered pressures had (with Philadelphia as an exception) an approximate range of 12.5 to 14 psi. The Philadelphia fuel had a value of 16.1 psi. The weathered values varied from about 10 to 11 psi indicating losses in ERVP ranging from about 2.0 to 5.1 psi for the 48-hour period.

Figures 1 through 5 are the plotted vapor pressure results for fuels which were tested simultaneously. It should be noted that the differences in equilibration time (from initial sample to $t = 0$) are due to changes in test cell heating capabilities. An initial malfunction in the system was responsible for longer equilibration periods as seen in the Denver-Wichita plot (figure 4). These times were reduced to around 10 hours following repairs. Cell temperatures at times reached 120° F during this period, but careful modulation assured no fuel temperature excursions from the target values. A linear regression analysis was conducted on the results for the winter grade fuels. From these results there appears to be a strong relationship between the change in vapor pressure and the initial RVP; that is, the higher the initial RVP, the greater the change due to aging. However, this relationship is also affected by fuel compositional differences. The data suggest that fuels with similar initial vapor pressures, i.e., Denver-Wichita and Rockville-San Diego, do not necessarily weather similarly. These differences would appear to be attributable to compositional differences. In general, most of the vapor pressure decreases occurred before the 48-hour weathering point.

Table I presents octane changes (both RON and MON) for these ten high vapor pressure winter fuels. Decreases in octane quality due to weathering appeared to be minimal and were generally less than 0.3 octane number. Most of these data were within experimental repeatability. An exception is seen with the winter Philadelphia regular unleaded fuel. A decrease of 0.7 in MON was noted and as can be seen in the compositional data, is attributed to the high initial content of butane.

Figures 6 through 15 show changes in the fuels' distillation character due to the controlled weathering conditions. The fuels all exhibited similar trends, with the major effect due to loss of volatile front-end components.

Increases in fuel initial boiling point (IBP) attributable to the 110° F soak ranged from 1° to 8° F. Ten-volume percent distilled level changes varied from a low of 12° F for the Sacramento fuel to a high of 16° F for the unleaded fuel from Wichita.

Table II of the fuels showed similar trends for the most part, with the high vapor pressure Philadelphia fuel exhibiting the largest changes in boiling character. Distillation temperature increases for this fuel ranged to more than 10° F between the 10- and 50-volume percent distilled points. Again, the larger increases in this fuel are attributable to losses of a large amount of butane content in the original fuel.

Tables 3 through 12 are fuel compositions for the individual fuels. These are results of gas chromatographic analyses conducted on the initial and 48-hour samples. These GC data are presented as volume percent summations as a function of both carbon number and compound class. A listing of compound specific analyses for each summer and winter fuel, original and weathered, are contained in reference 1. In general, as might be expected, most of the changes occur in the C₁ to C₅ range containing the most volatile materials, i.e., butanes, and pentanes. Note that when reviewing tables 3 through 12, relative changes should be kept in mind; as one component decreases, the relative percentage of the others increase.

As an example, the 16.1 psi Philadelphia fuel exhibited the largest changes in vapor pressure, octane, and distillation character. Table 4 presents the compositional summaries from samples taken before and after weathering. By far, the largest total change is with the C₄ compounds. The very high initial vapor pressure would suggest that the volatile materials lost were butane and isopentane. The specific component listing in reference 1 indicates a high initial butane content.

SUMMER-FUEL FUELS.

The summer fuels tested were procured from geographic locations similar to those of the winter fuels. Both regular and premium unleaded gasolines were obtained, and as would be discovered, a gasohol fuel was included. Table 13 shows the effect of a controlled 110° F soak on the vapor pressures. Unweathered fuel RVP values were from about 8.5 to 11 psi. Decreases in vapor pressures due to weathering ranged from a low of 0.5 psi for Wichita samples to a high of 2.0 psi for Duluth. As with the winter fuels, most of the decreases occurred within 12 hours, and the drop in RVP appears to be marginally dependent on the initial RVP of the summer grade blends, with the fuel composition affecting the overall decline.

Octane quality changes are presented in table 14. Motor octane results showed no degradation for most of the fuels. Only the premium unleaded Sacramento fuel tests indicated a significant octane decrease of 0.7.

Figures 16 through 25 contain information on the summer fuel distillation character before and after weathering. For most cases, there were barely discernible differences in fuel boiling range due to weathering. IBP changes were minimal. The Houston fuel exhibited the most change with 5, 10, and 20 percent points increasing by about 10° F after weathering. This is not unexpected for these fuels since they contain far lower quantities of the more volatile front-end components normally used for vapor pressure enhancement. Specific alcohol analysis was conducted with the New Orleans fuel. Results showed 10-volume percent ethanol, thus accounting for the unusual shape of the distillation curves--the boiling point for ethanol is 173° F.

Tables 15 through 25 contain fuel compositional summaries for the summer fuels. As with the winter fuel results, the changes occur mostly in the front ends, from C₁ to C₅. Again, the specific component results for these fuels are contained in reference 1. It should be noted that the relatively small component losses for these fuels had essentially no effects on their octane and distillation characteristics.

CONCLUSIONS

Tests were conducted to measure the effect of aging automobile gasoline on fuel volatility and octane characteristics. Winter and summer grade fuels were acquired from various locations in the continental United States.

It can be concluded that in most cases changes in automobile gasoline octane quality due to aging fuels at 110° F for 48 hours would be negligible for both summer and winter fuels. The only exceptions found in these tests were due to one case of a relatively high butane concentration in the fuel and in another a sample container leaked following aging but prior to testing for the octane rating.

The magnitude of decrease in volatility, as characterized by Reid Vapor Pressure (RVP) was somewhat dependent on the initial test fuel RVP. However, fuel with similar initial vapor pressures do not necessarily age in a similar manner. Volatility decreases due to aging are dependent on the type and quantity of volatile hydrocarbon components found in the fuel.

Decreases in RVP due to aging, for both summer and winter fuels, occurred primarily during the 12-hour period following equilibration at 110° F. Changes occurring between 12 and 48 hours were within method repeatability.

Aging of the summer-grade fuels produced only minor increases in the distillation temperatures. Increases in the initial boiling point and distillation curve were more pronounced for the winter-grade fuels. These increases were most evident in the front end (low molecular weight-low boiling) point range of the distillation curve. The winter grade Philadelphia gasoline, which contained a very high butane concentration, exhibited the greatest loss in volume. The changes measured in these experiments are similar to results from static studies contained in references 2, 3, and 4.

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TABLE 1. - Vapor pressure versus time

Fuel	Original	Equivalent Reid Vapor Pressure (psi)			
		0	12	24	48
Houston, TX	12.51	11.69	11.31	10.97	10.65
Sacramento, CA	12.51	11.46	10.99	11.10	10.61
Philadelphia, PA	16.14	12.11	11.37	11.16	10.78
New Orleans, LA	12.66	11.61	11.10	11.03	10.80
Rockville, MD	12.86	10.99	10.70	10.32	10.13
San Diego, CA	12.98	11.48	11.18	10.95	10.87
Denver, CO	14.06	12.36	11.73	11.27	10.84
Wichita, KS	14.08	12.08	11.69	11.54	11.37
Ft. Lauderdale, FL	11.98	10.19	10.15	10.04	9.81
Chicago, IL	13.93	11.82	11.44	11.37	10.87

TABLE 2. - Octane ratings

Fuel	RON			MON		
	Initial	Final	Diff.	Initial	Final	Diff.
Houston, TX	91.6	91.5	0.1	82.6	82.4	0.2
Sacramento, CA	92.0	91.7	0.3	82.6	82.4	0.2
Philadelphia, PA	92.1	91.7	0.4	81.5	80.8	0.7
New Orleans, LA	92.3	92.3	0.0	86.2	86.1	0.1
Rockville, MD	91.7	91.4	0.3	82.3	82.2	0.1
San Diego, CA	92.3	92.1	0.2	82.8	82.5	0.3
Denver, CO	89.0	88.6	0.4	80.5	80.1	0.4
Wichita, KS	91.8	91.7	0.1	82.8	82.5	0.3
Ft. Lauderdale, FL	91.6	91.6	0.0	82.2	82.1	0.1
Chicago, IL	91.3	91.3	0.0	82.4	82.3	0.1

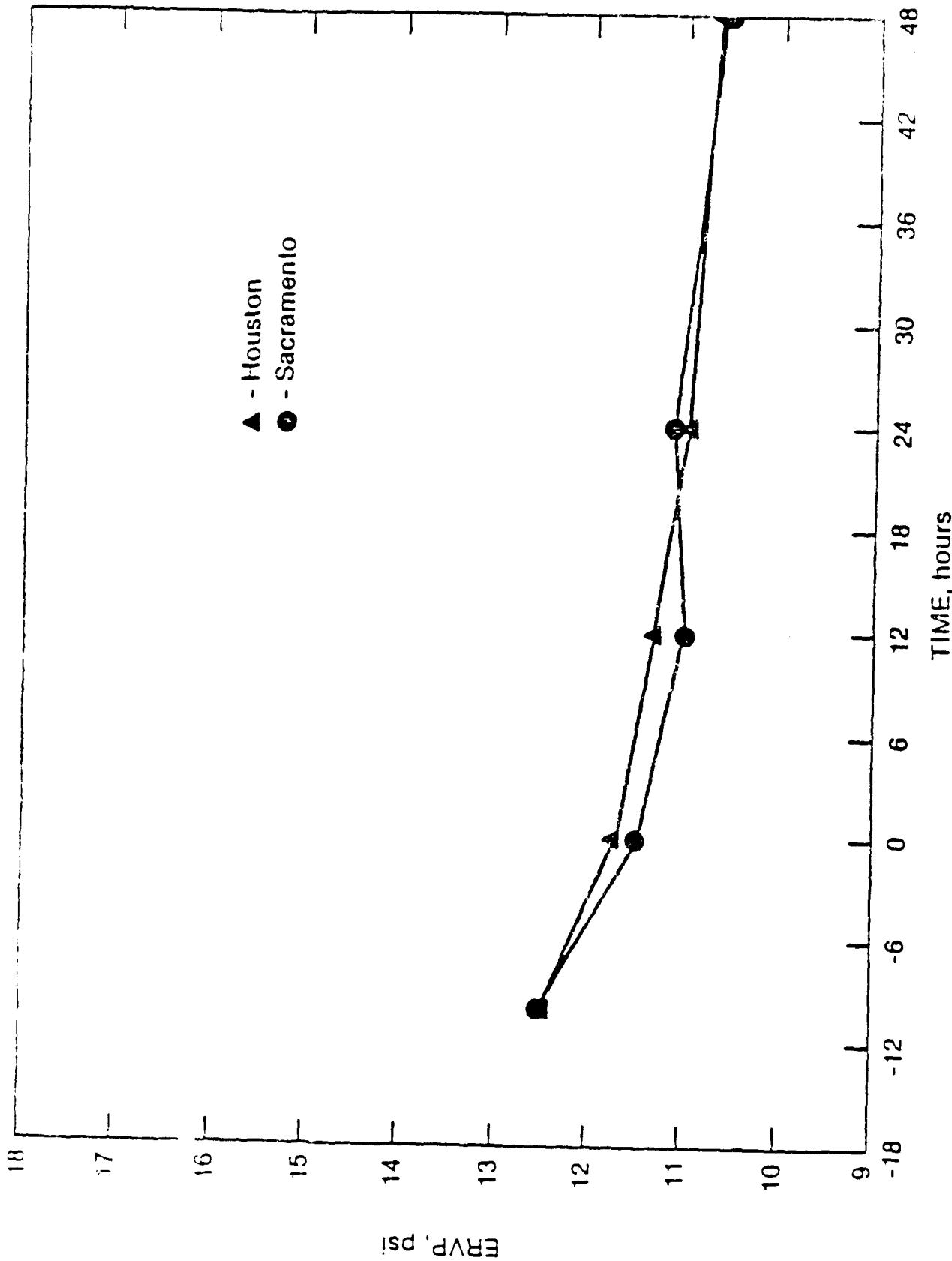
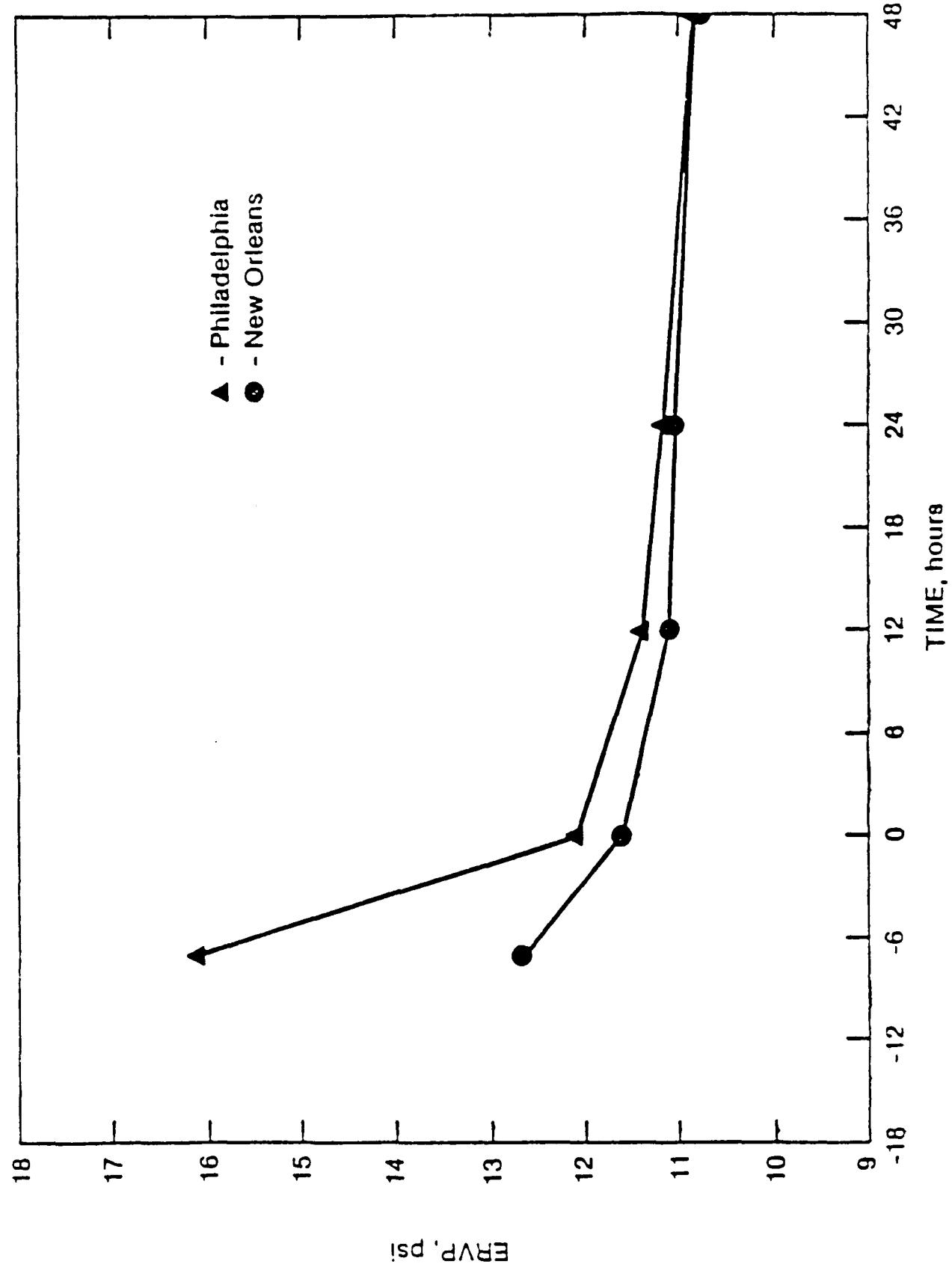


FIGURE 1. - Vapor pressure history, winter fuels from Houston and Sacramento.



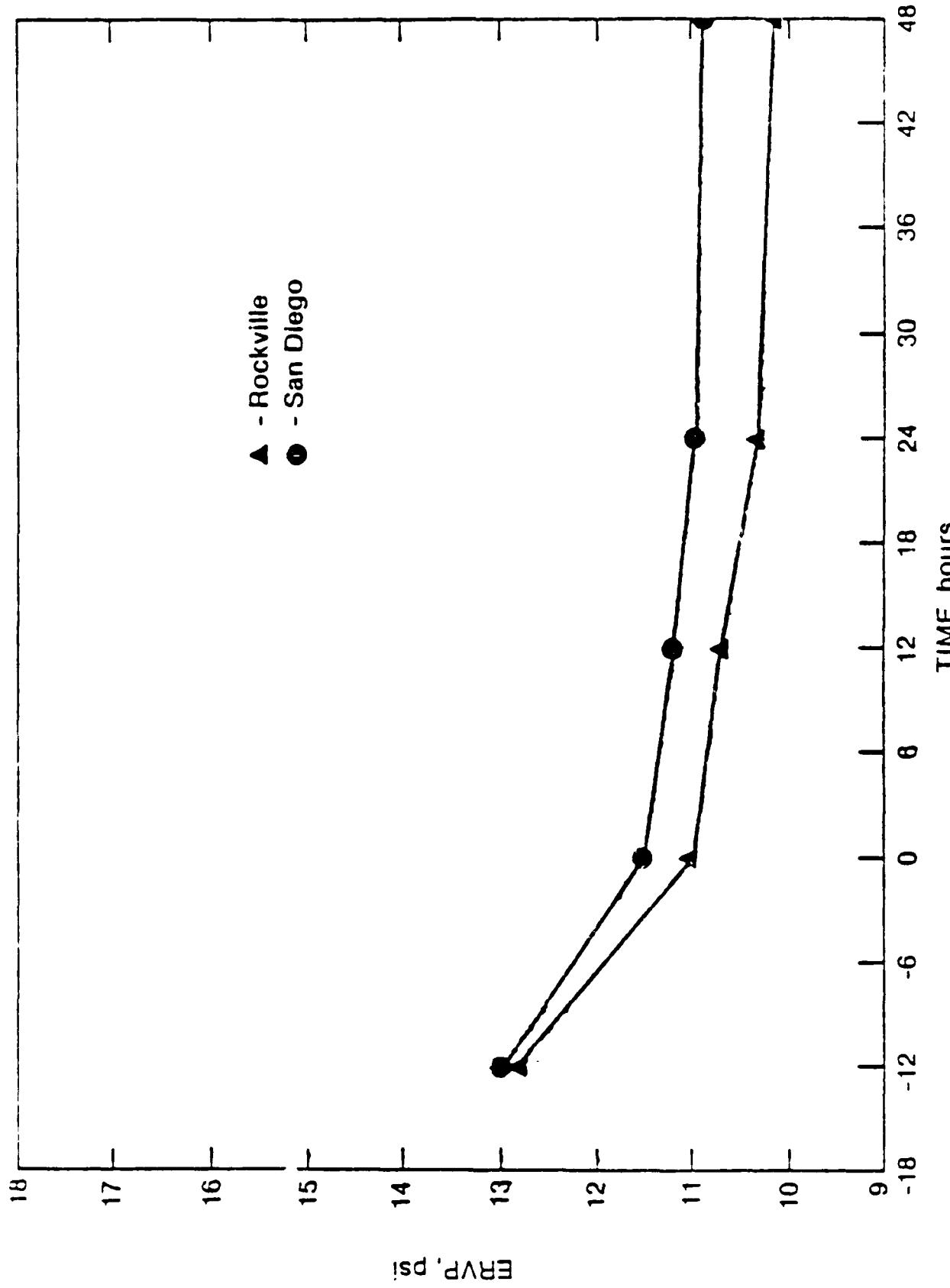


FIGURE 3. - Vapor pressure history, winter fuels from Rockville and San Diego.

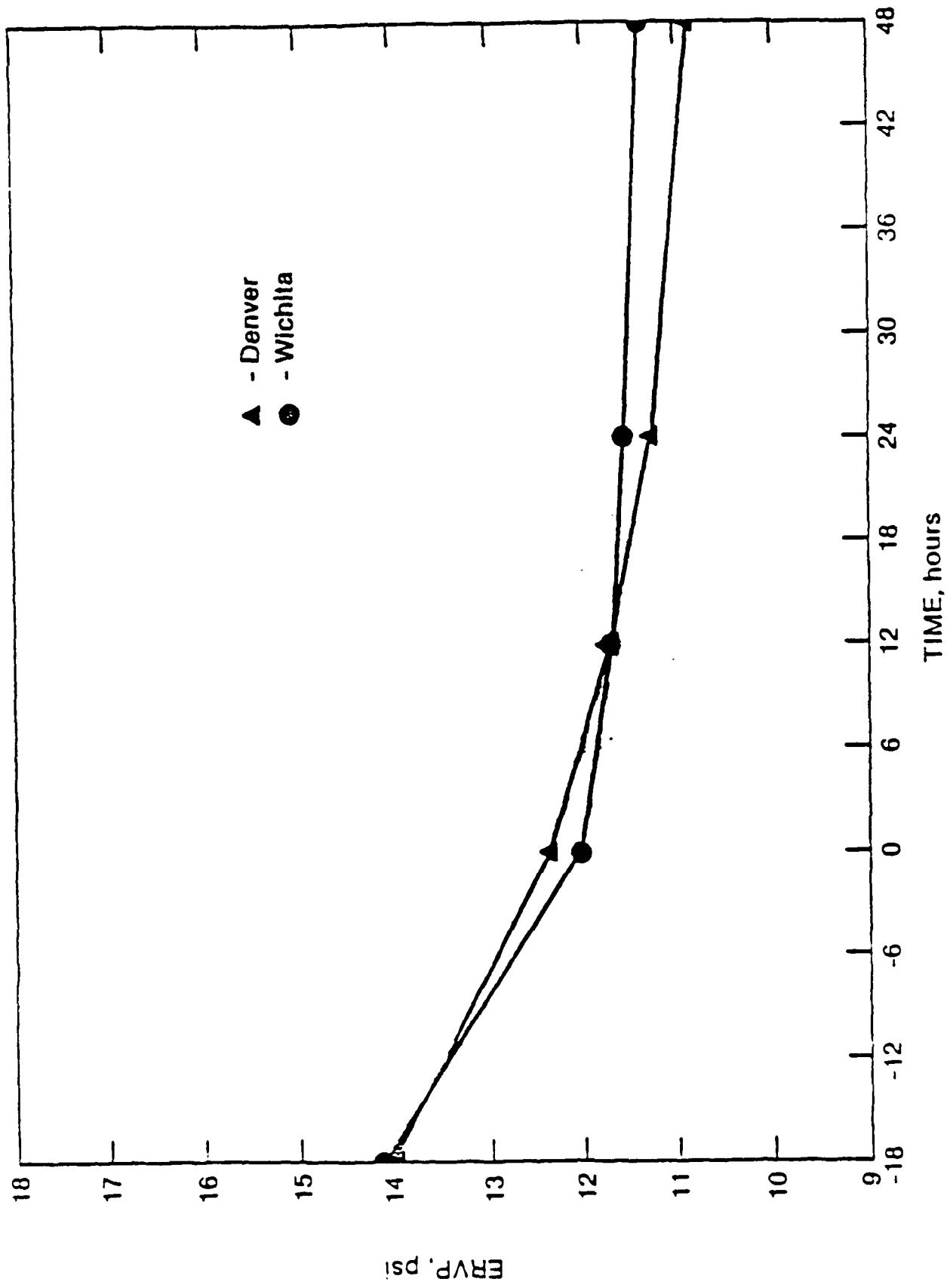


FIGURE 4. - Vapor pressure history, winter fuels from

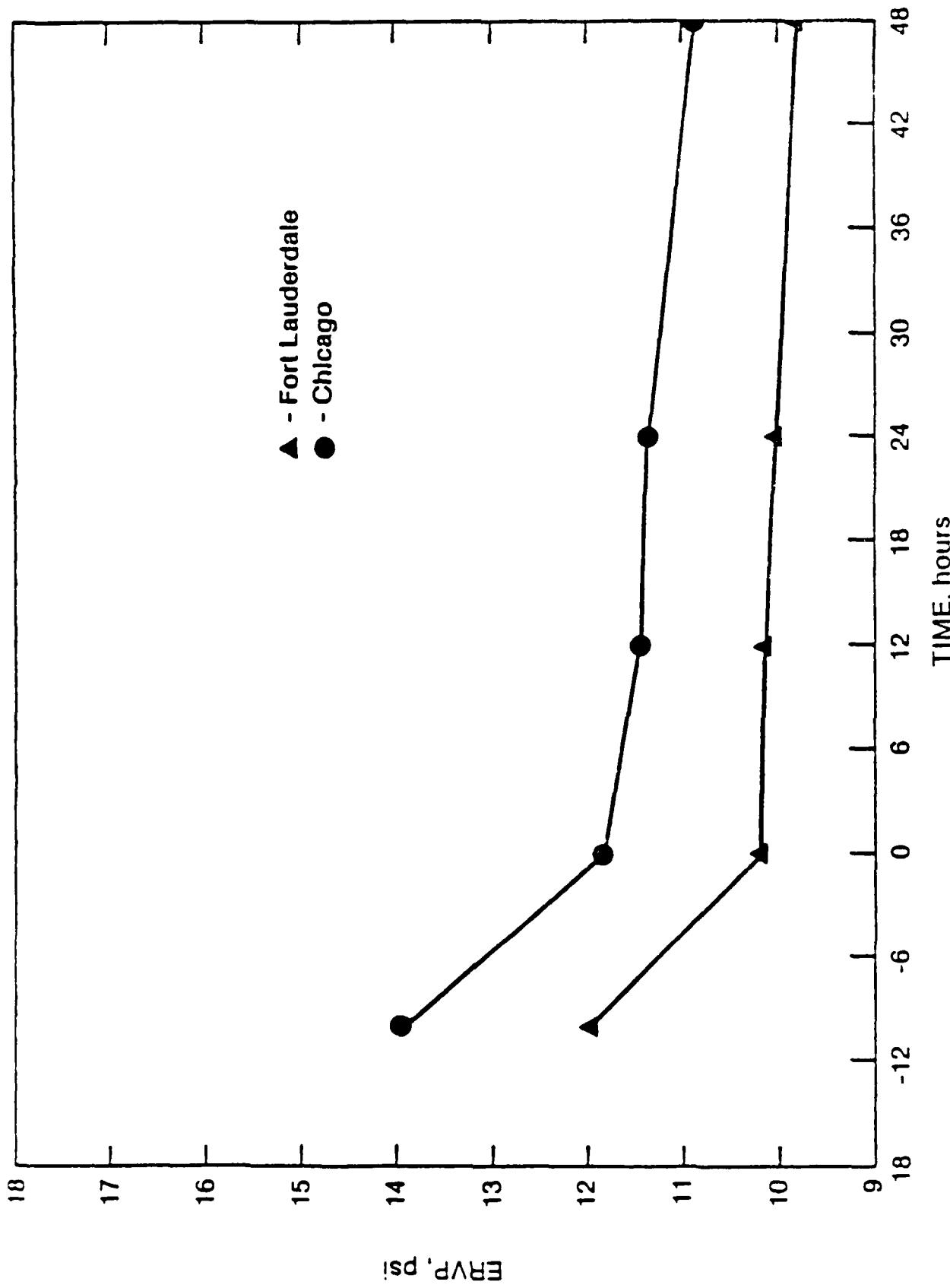


FIGURE 5. - Vapor pressure history, winter fuels from
Ft. Lauderdale and Chicago.

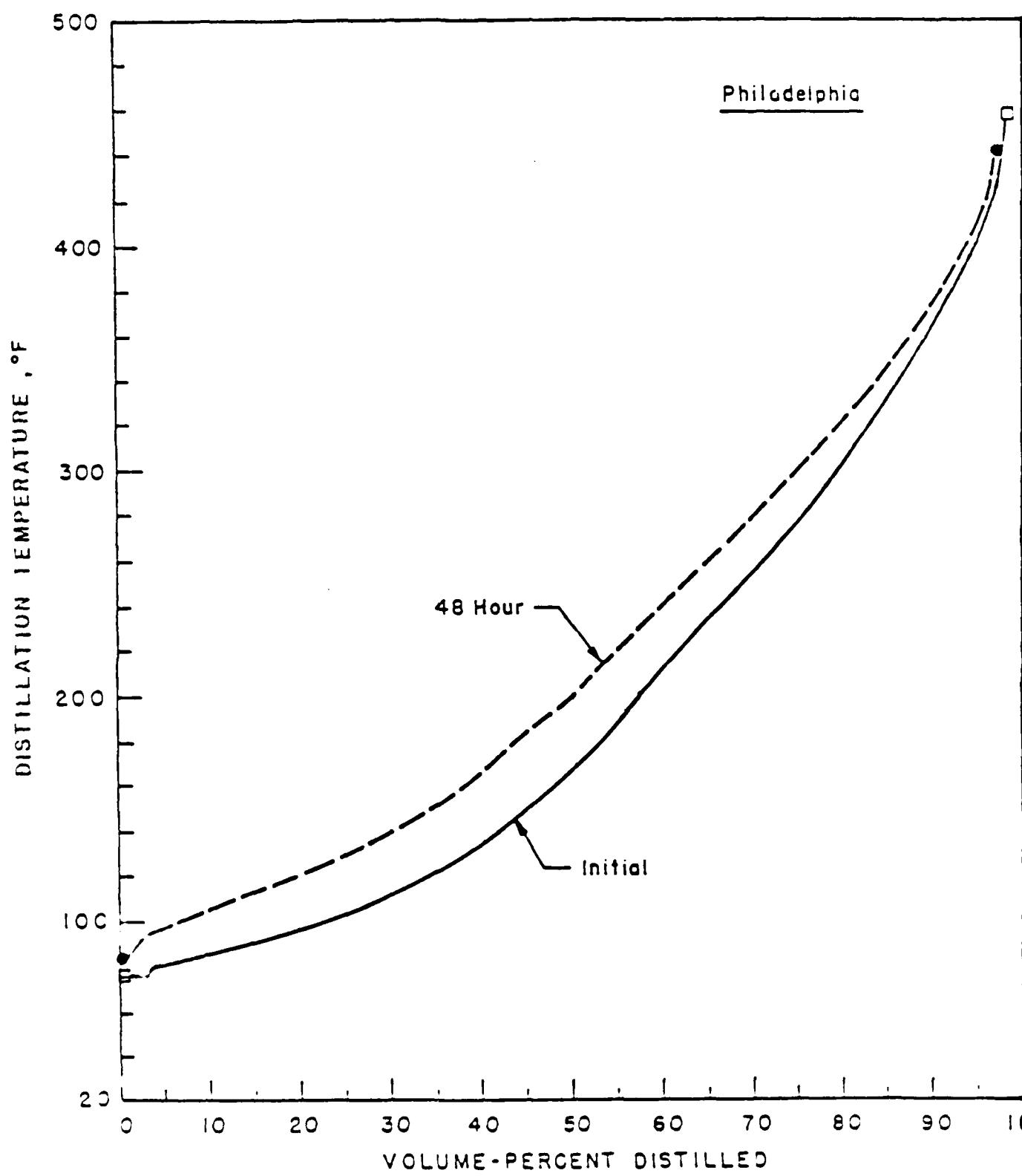


FIGURE 6. - Changes in distillation character due to weathering, winter fuels from Philadelphia.

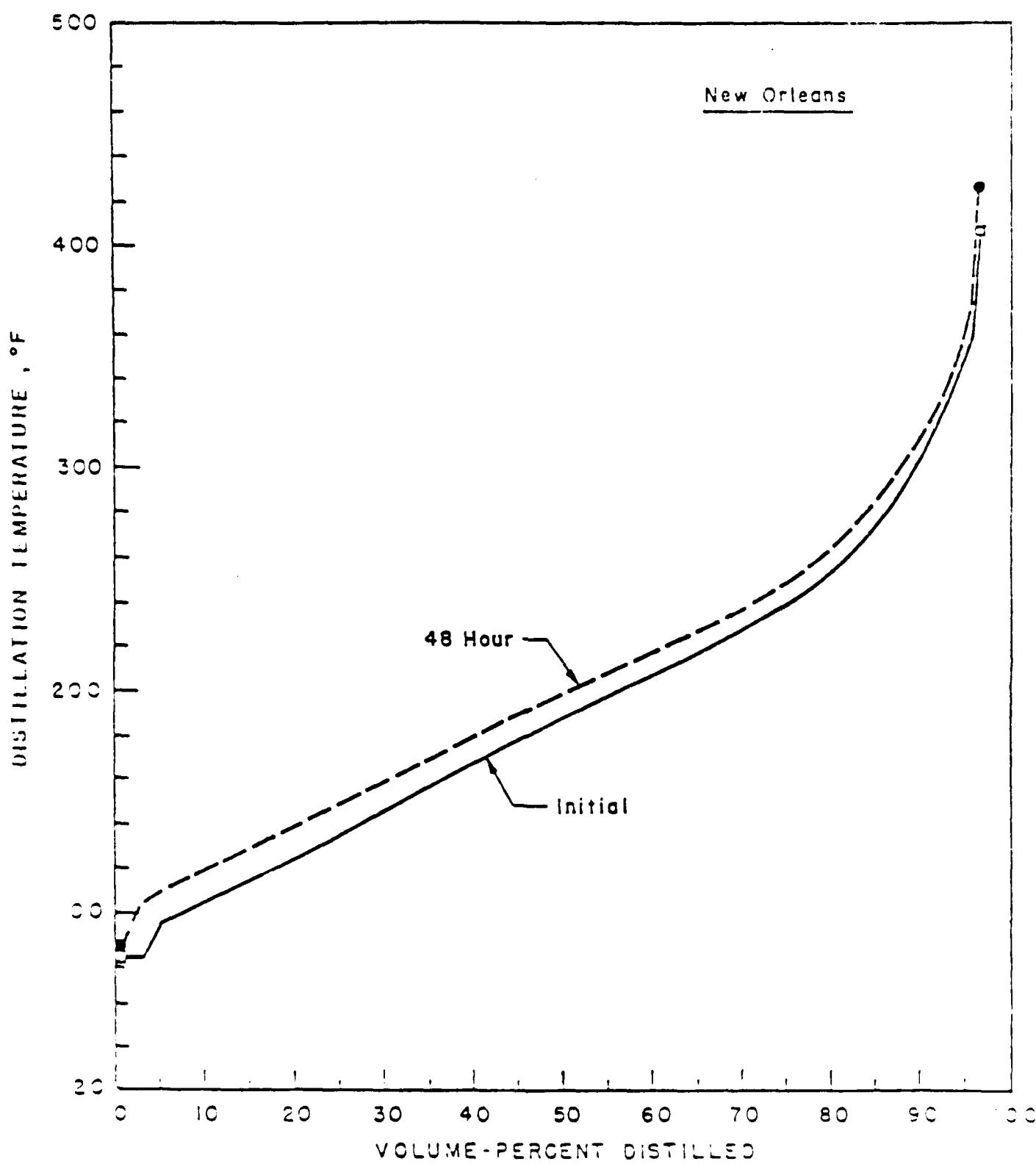


FIGURE 7. - Changes in distillation character due to weathering,
winter fuels from New Orleans.

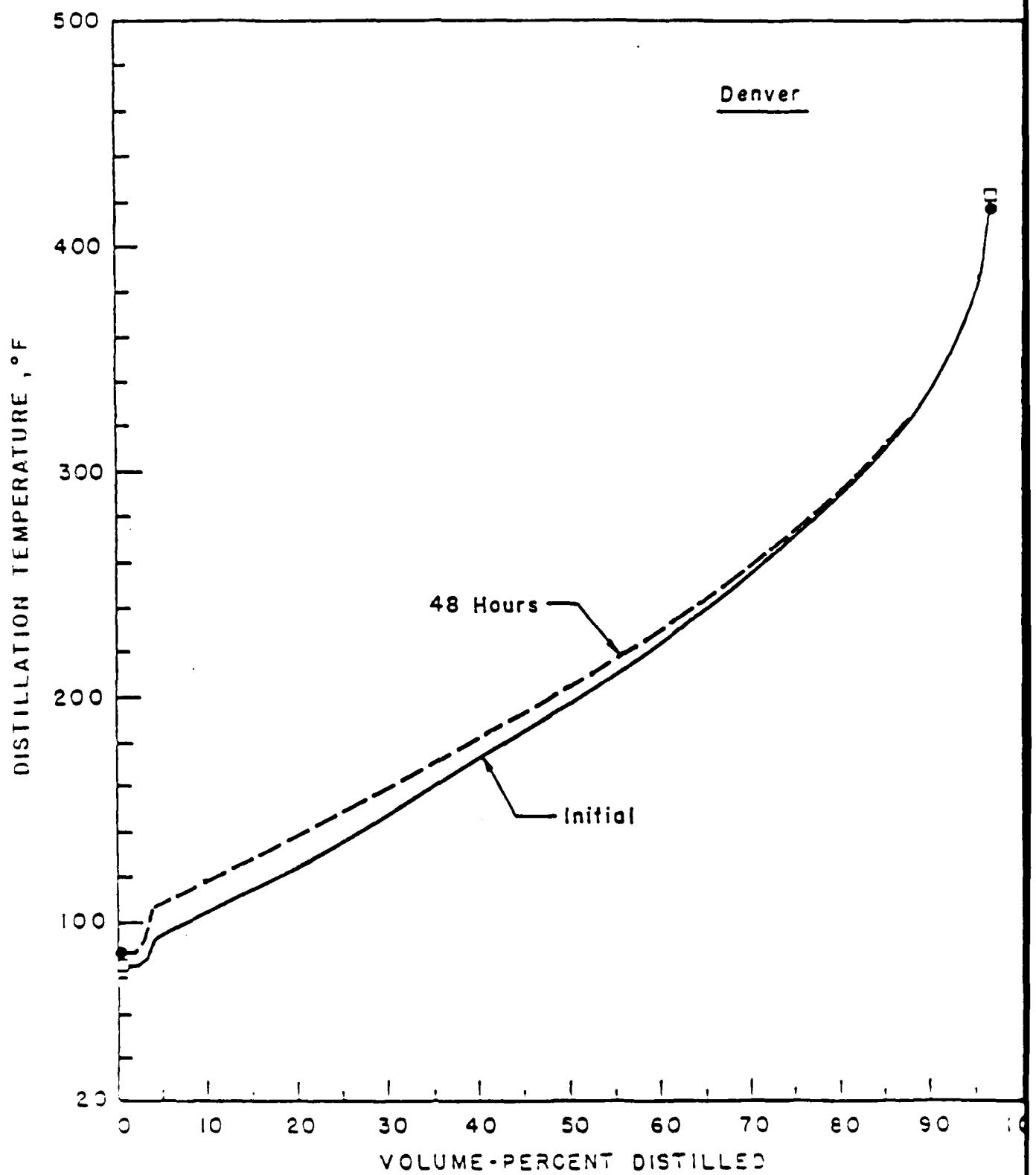


FIGURE 8. - Changes in distillation character due to weathering, winter fuels from Denver.

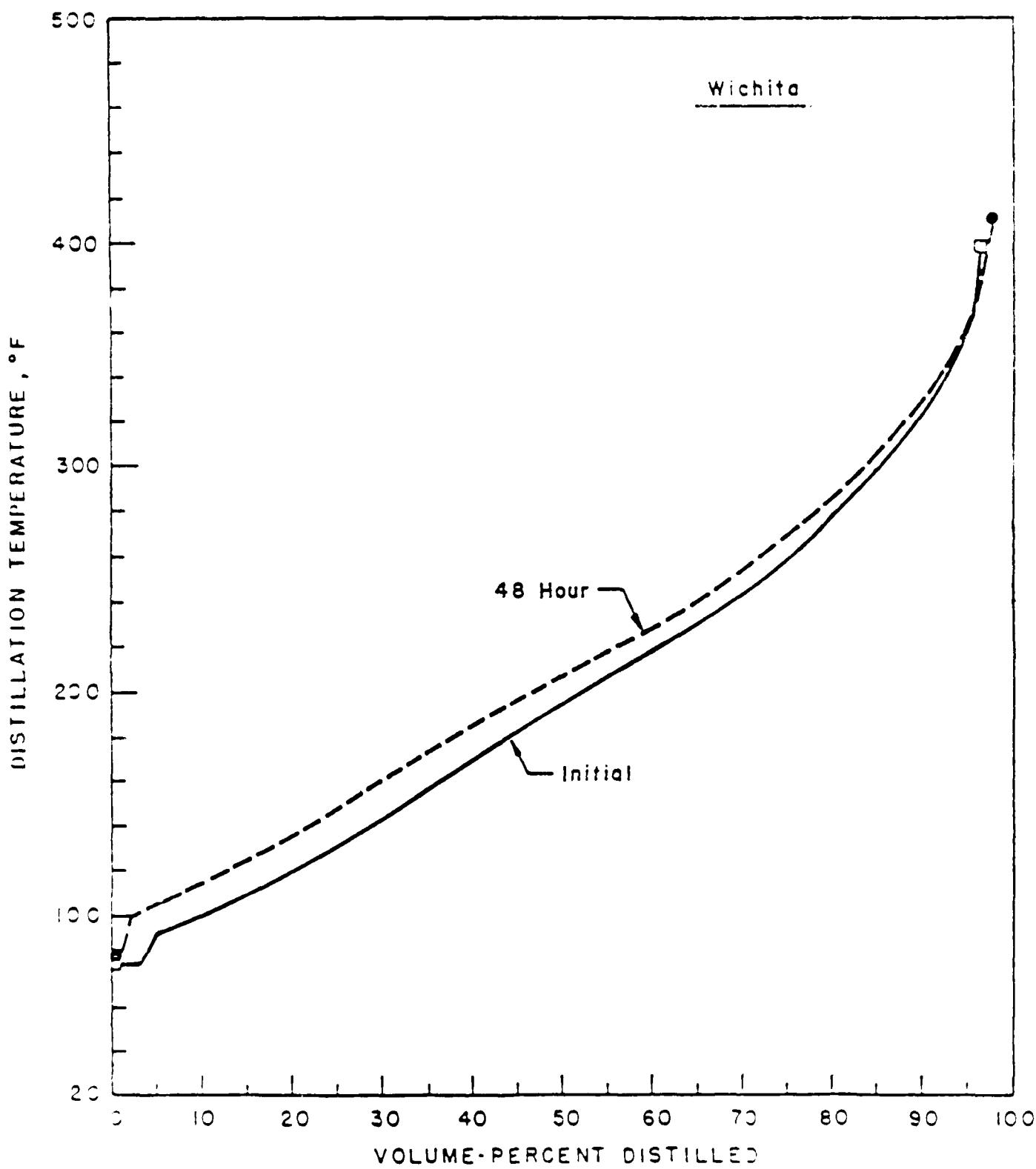


FIGURE 9. - Changes in distillation character due to weathering,
winter fuels from Wichita.

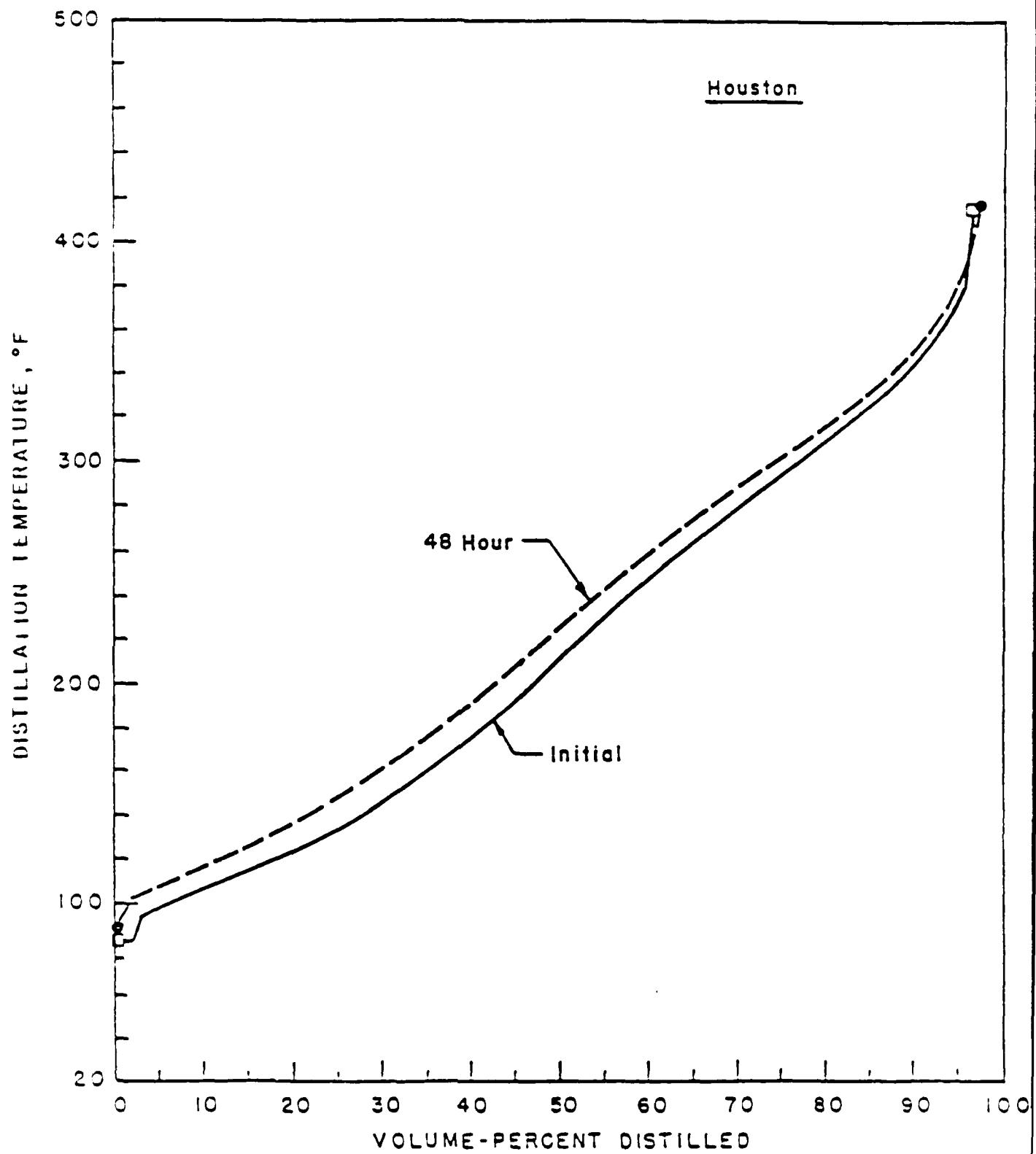


FIGURE 10. - Changes in distillation character due to weathering, winter fuels from Houston.

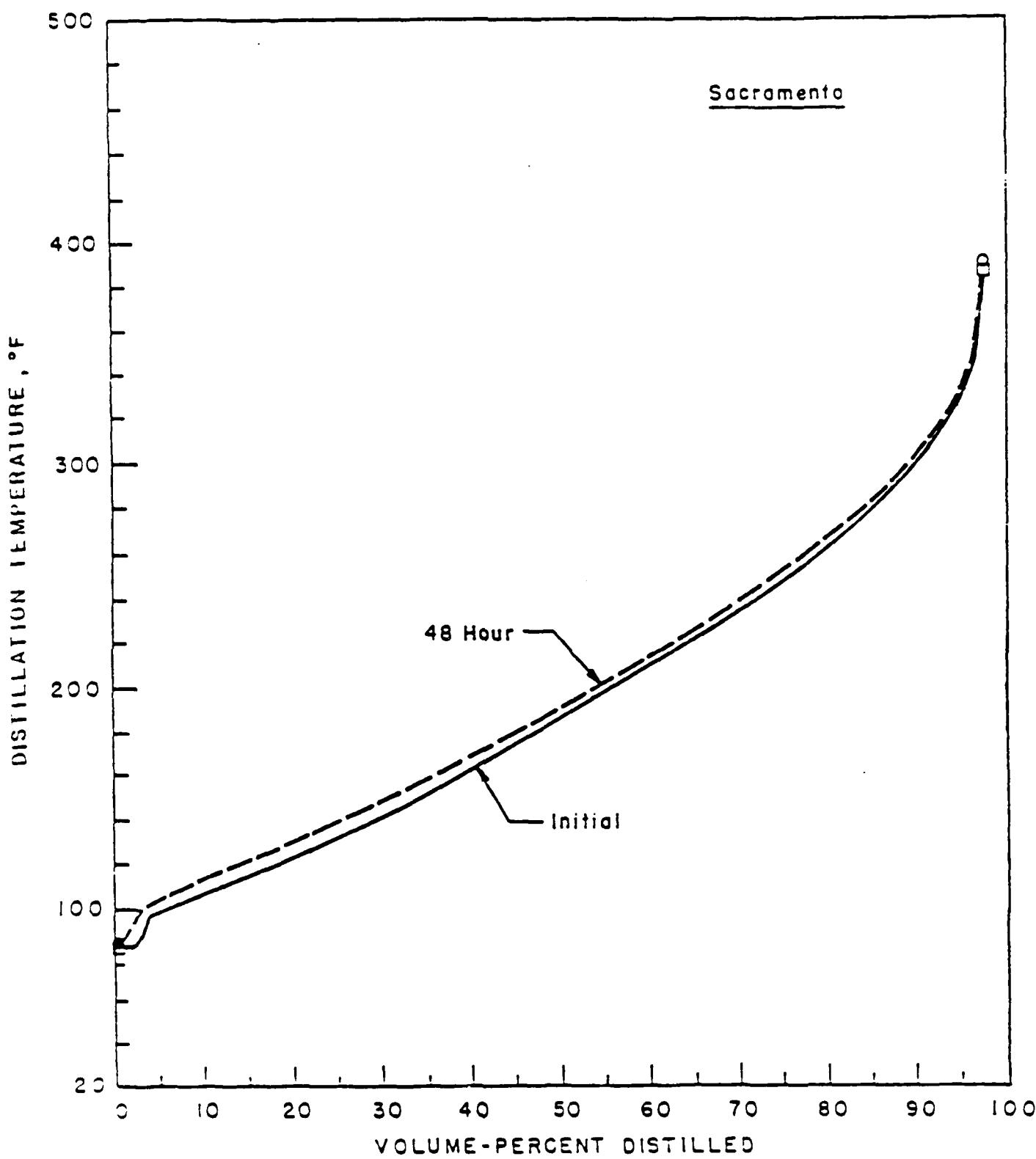


FIGURE 11. - Changes in distillation character due to weathering,
winter fuels from Sacramento.

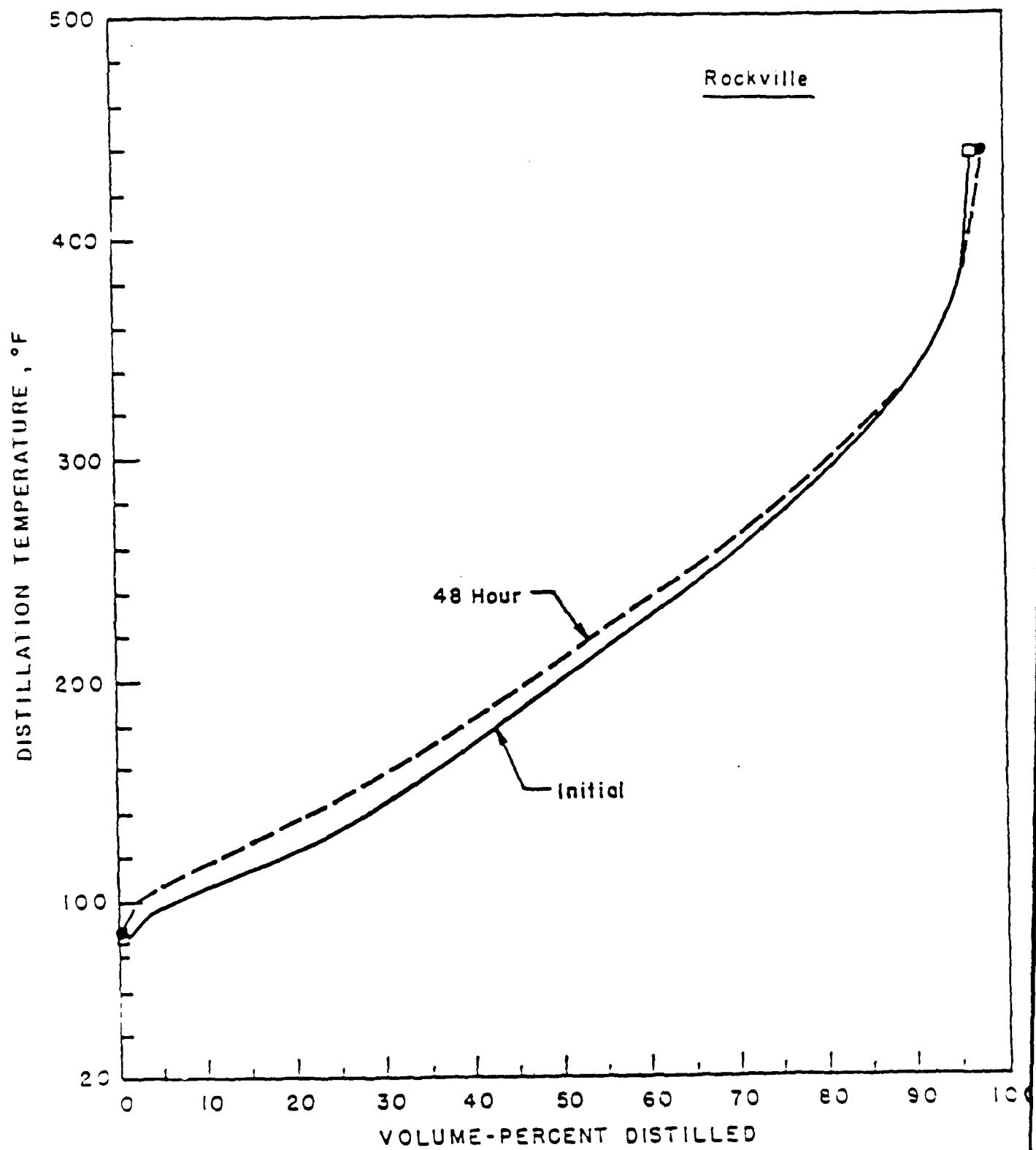


FIGURE 12. - Changes in distillation character due to weathering,
winter fuels from Rockville.

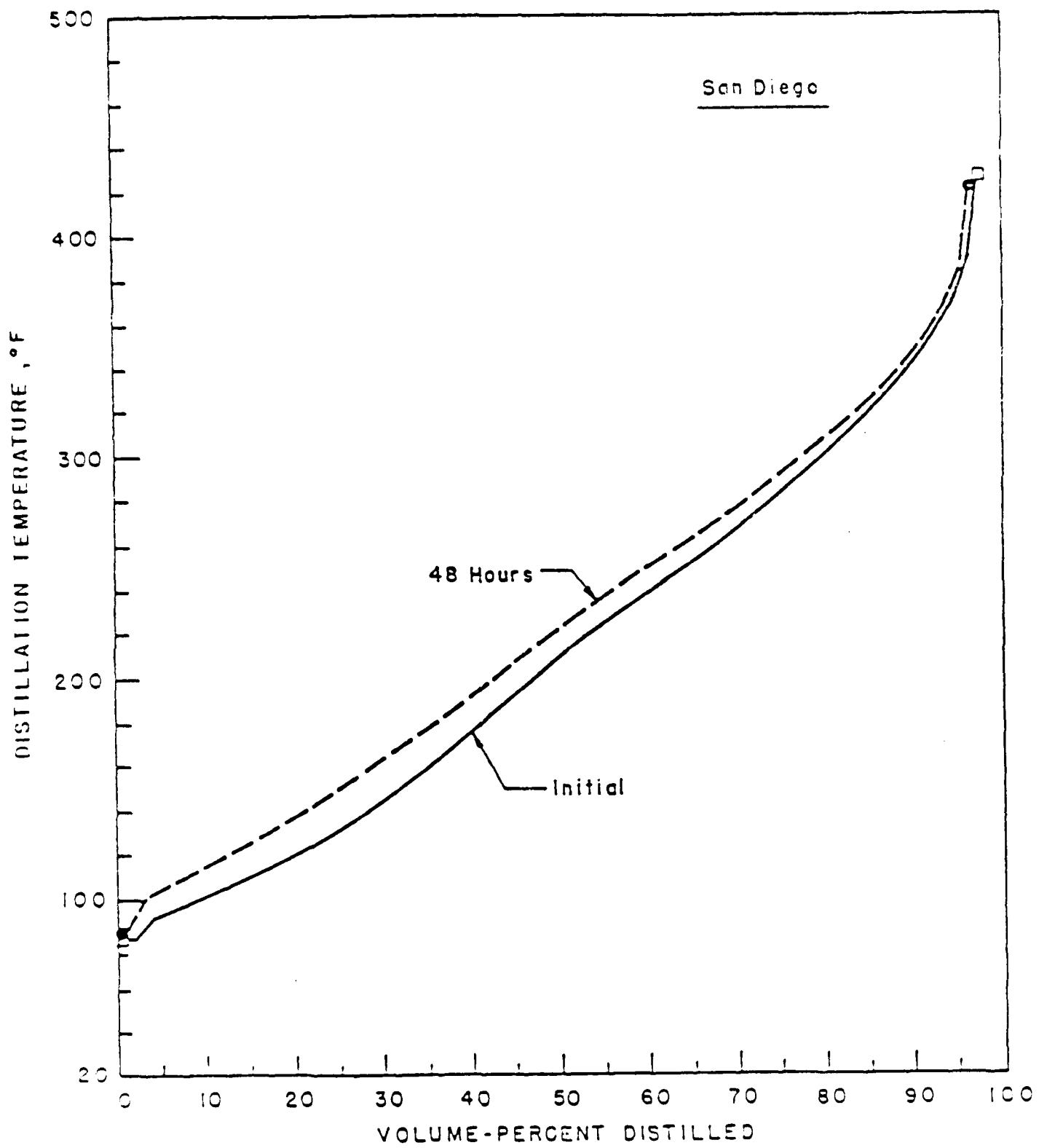


FIGURE 13. - Changes in distillation character due to weathering,
winter fuels from San Diego.

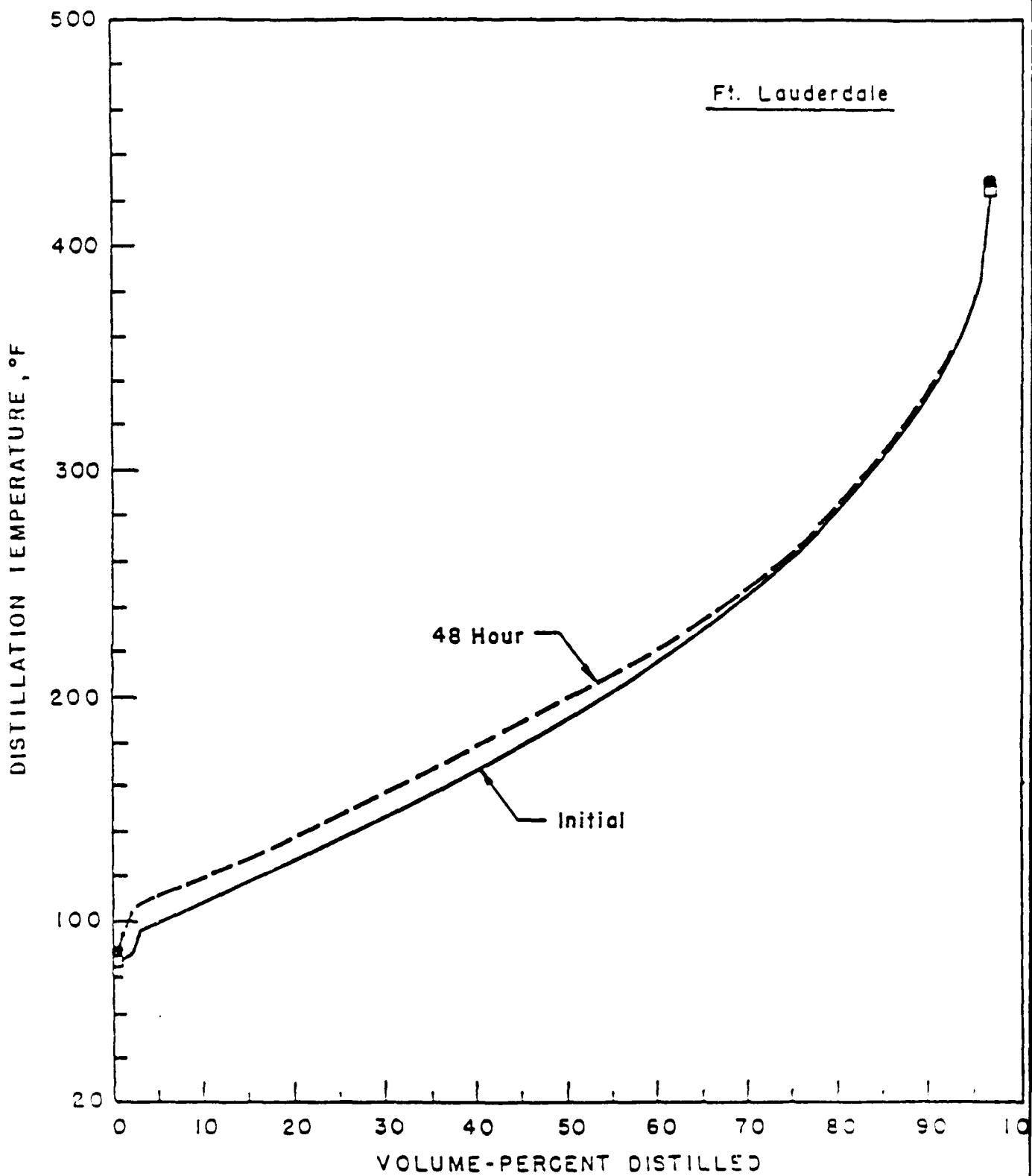


FIGURE 14. - Changes in distillation character due to weathering, winter fuels from Ft. Lauderdale.

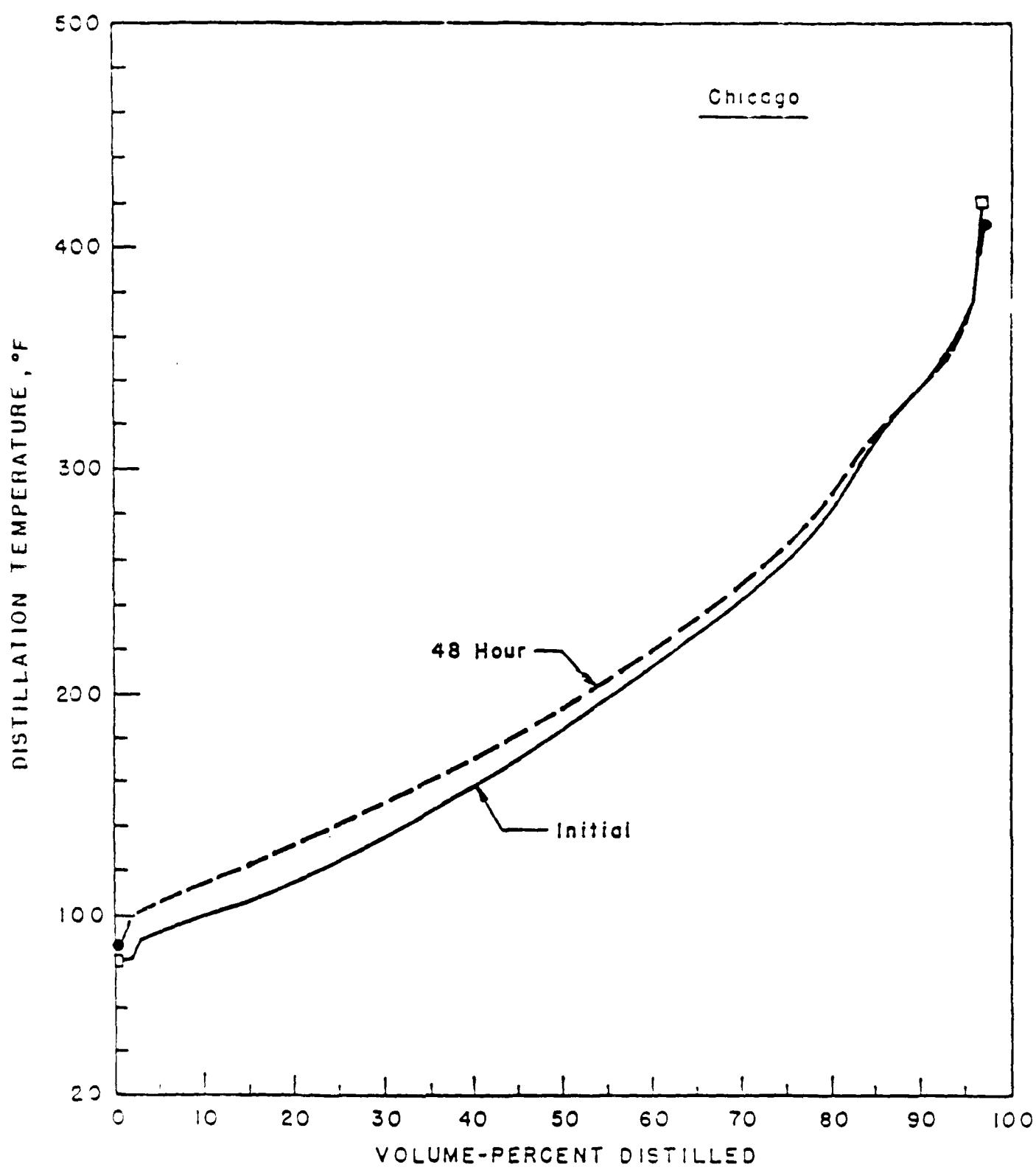


FIGURE 15. - Changes in distillation character due to weathering, winter fuels from Chicago.

TABLE 3. - Fuel composition summary - New Orleans - winter

Carbon No.	Volume-percent Summation by Carbon Number and Compound Class					<u>Initial</u>
	Normal	Paraffins Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.12	0.00	0.00	0.02	0.00	0.13
4	9.54	2.26	0.00	0.88	0.00	12.69
5	5.94	8.65	0.12	4.52	0.00	19.23
6	4.27	8.01	1.42	1.51	1.03	16.24
7	1.47	8.41	2.10	2.68	3.68	18.33
8	0.57	16.88	0.69	0.03	4.45	22.63
9	0.12	2.83	0.04	0.00	3.06	6.05
10	0.05	2.20	0.00	0.00	2.22	4.47
11	0.05	0.02	0.00	0.00	0.15	0.22
12	0.00	0.00	0.00	0.00	0.00	0.00
Total	22.13	49.27	4.36	9.64	14.60	100.00

Average Molecular Weight = 88.64

Average Density - .702

Average Carbon Number = 6.29

H/C Ratio = 2.06

48 Hours

Carbon No.	Volume-percent Summation by Carbon Number and Compound Class					<u>48 Hours</u>
	Normal	Paraffins Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.05	0.00	0.00	0.01	0.00	0.06
4	7.55	1.59	0.00	0.70	0.00	9.85
5	5.65	8.00	0.11	4.57	0.00	18.33
6	4.26	7.93	1.43	1.53	1.11	16.25
7	1.50	8.45	2.10	2.72	4.01	18.78
8	0.59	19.48	0.87	0.04	4.61	25.59
9	0.12	3.14	0.00	0.00	3.19	6.45
10	0.05	2.28	0.00	0.00	2.15	4.48
11	0.05	0.02	0.00	0.00	0.14	0.21
12	0.00	0.00	0.00	0.00	0.00	0.00
Total	19.82	50.87	4.51	9.57	15.21	100.00

Average Molecular Weight = 90.69

Average Density - .708

Average Carbon Number = 6.44

H/C Ratio = 2.04

TABLE 4. - Fuel composition summary - Chicago - winter

Volume-percent Summation by Carbon Number and Compound Class

Carbon No.	<u>Initial</u>					<u>Total</u>
	<u>Normal</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	
Iso						
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.17	0.00	0.00	0.02	0.00	0.18
4	11.68	1.57	0.00	1.35	0.00	14.60
5	6.23	10.56	0.19	4.29	0.00	21.28
6	3.12	11.44	2.57	1.74	1.76	20.63
7	1.73	4.56	1.26	2.07	9.02	18.65
8	0.58	5.75	1.17	0.10	3.18	10.78
9	0.14	1.04	0.00	0.00	7.56	8.73
10	0.10	0.20	0.00	0.00	4.22	4.53
11	0.10	0.03	0.00	0.00	0.49	0.62
12	0.00	0.00	0.00	0.00	0.00	0.00
<u>Total</u>	<u>23.85</u>	<u>35.15</u>	<u>5.19</u>	<u>9.58</u>	<u>26.23</u>	<u>100.00</u>

Average Molecular Weight = 85.92

Average Density - .715

Average Carbon Number = 6.16

H/C Ratio = 1.93

48 Hours

Carbon No.	<u>48 Hours</u>					<u>Total</u>
	<u>Normal</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	
Iso						
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.05	0.00	0.00	0.00	0.00	0.05
4	7.98	0.88	0.00	0.93	0.00	9.79
5	5.82	9.48	0.19	4.01	0.00	19.49
6	4.19	11.73	2.78	2.49	1.87	23.06
7	1.88	4.96	1.37	2.28	9.89	20.39
8	0.63	6.41	0.77	0.11	3.55	11.48
9	0.15	1.23	0.00	0.00	8.35	9.74
10	0.12	0.26	0.00	0.00	4.75	5.12
11	0.11	0.03	0.00	0.00	0.73	0.87
12	0.00	0.00	0.00	0.00	0.00	0.00
<u>Total</u>	<u>20.93</u>	<u>34.98</u>	<u>5.11</u>	<u>9.82</u>	<u>29.14</u>	<u>100.00</u>

Average Molecular Weight = 88.87

Average Density - .727

Average Carbon Number = 6.39

H/C Ratio = 1.88

TABLE 5. - Fuel composition summary - Ft. Lauderdale - winter

Carbon No.	Normal	Initial					Total
		Paraffins Iso	Naphthenes	Olefins	Aromatics		
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3	0.14	0.00	0.00	0.05	0.00	0.19	
4	8.12	1.59	0.00	1.20	0.00	10.92	
5	5.78	10.71	0.17	4.19	0.00	20.85	
6	3.40	10.87	2.64	3.04	2.29	22.25	
7	1.66	5.75	1.52	2.59	8.31	19.83	
8	0.45	5.92	0.77	0.06	6.45	13.65	
9	0.12	1.63	0.02	0.00	6.09	7.86	
10	0.08	0.25	0.00	0.00	3.67	4.00	
11	0.07	0.00	0.00	0.00	0.40	0.46	
12	0.00	0.00	0.00	0.00	0.00	0.00	
Total	19.81	36.73	5.12	11.13	27.21	100.00	

Average Molecular Weight = 87.39

Average Density - .720

Average Carbon Number = 6.27

H/C Ratio = 1.90

Carbon No.	Normal	48 Hours					Total
		Paraffins Iso	Naphthenes	Olefins	Aromatics		
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3	0.06	0.00	0.00	0.02	0.00	0.08	
4	5.41	1.10	0.00	0.92	0.00	7.43	
5	5.42	10.00	0.17	4.03	0.00	19.61	
6	3.37	10.79	2.72	3.25	2.56	22.68	
7	1.71	6.44	1.75	2.88	8.46	21.24	
8	0.42	6.32	0.89	0.08	8.12	15.83	
9	0.12	2.10	0.06	0.00	5.86	8.14	
10	0.07	0.37	0.00	0.00	3.59	4.03	
11	0.05	0.13	0.00	0.00	0.72	0.90	
12	0.00	0.00	0.00	0.00	0.05	0.05	
Total	16.61	37.25	5.59	11.19	29.36	100.00	

Average Molecular Weight = 89.78

Average Density - .730

Average Carbon Number = 6.46

H/C Ratio = 1.87

TABLE 6. - Fuel composition summary - Philadelphia - winter

Carbon No.	Volume-percent Summation by Carbon Number and Compound Class					Initial <u>Total</u>
	Normal	Paraffins Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.06	0.00	0.00	0.01	0.00	0.07
4	9.23	3.19	0.00	5.09	0.00	17.51
5	0.55	12.86	0.24	6.77	0.00	29.43
6	1.70	6.46	1.61	5.27	0.44	15.49
7	0.85	2.90	1.42	3.62	3.50	12.29
8	0.37	3.34	1.65	0.16	5.21	10.74
9	0.14	2.89	0.09	0.00	4.96	8.08
10	0.11	0.70	0.00	0.00	3.97	4.78
11	0.15	0.08	0.00	0.00	0.89	1.13
12	0.15	0.16	0.00	0.00	0.18	0.48
Total	22.31	32.59	5.02	20.93	19.15	100.00

Average Molecular Weight = 83.51

Average Density - .699

Average Carbon Number = 5.96

H/C Ratio = 1.99

48 Hours

Carbon No.	Volume-percent Summation by Carbon Number and Compound Class					Total
	Normal	Paraffins Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.01	0.00	0.00	0.00	0.00	0.01
4	4.77	1.13	0.00	2.60	0.00	8.50
5	8.95	11.01	0.25	6.31	0.00	26.53
6	1.93	7.08	1.86	5.95	0.51	17.33
7	1.04	3.46	1.75	4.34	4.40	14.98
8	0.39	4.21	2.16	0.26	6.47	13.48
9	0.17	3.61	0.12	0.00	6.33	10.23
10	0.14	0.96	0.00	0.00	4.99	6.08
11	0.20	0.08	0.00	0.00	1.69	1.97
12	0.19	0.00	0.00	0.00	0.70	0.90
Total	17.78	31.54	6.13	19.46	25.09	100.00

Average Molecular Weight = 89.77

Average Density - .723

Average Carbon Number = 6.44

H/C Ratio = 1.91

TABLE 7. - Fuel composition summary - San Diego - winter

Carbon No.	Volume-percent Summation by Carbon Number and Compound Class					<u>Total</u>
	<u>Normal</u>	<u>Paraffins</u> <u>Iso</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.12	0.00	0.00	0.03	0.00	0.15
4	7.41	3.97	0.00	0.74	0.00	12.12
5	4.64	10.29	0.19	4.84	0.00	19.96
6	2.57	7.20	2.33	3.22	1.25	16.57
7	1.37	4.68	3.17	0.54	6.28	16.05
8	0.78	6.61	1.22	0.01	9.12	17.75
9	0.38	3.14	0.11	0.00	7.19	10.82
10	0.25	1.02	0.00	0.00	4.46	5.72
11	0.14	0.03	0.00	0.00	0.48	0.64
12	0.00	0.06	0.00	0.00	0.15	0.22
<u>Total</u>	<u>17.65</u>	<u>37.00</u>	<u>7.03</u>	<u>9.39</u>	<u>28.93</u>	<u>100.00</u>

Average Molecular Weight = 89.52

Average Density - .726

Average Carbon Number = 6.43

H/C Ratio = 1.89

Carbon No.	<u>48 Hours</u>					<u>Total</u>
	<u>Normal</u>	<u>Paraffins</u> <u>Iso</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.05	0.00	0.00	0.01	0.00	0.06
4	6.00	2.85	0.00	0.60	0.00	9.45
5	4.52	9.69	0.20	4.69	0.00	19.10
6	2.64	7.32	2.35	3.28	1.30	16.90
7	1.45	4.88	3.31	0.58	6.58	16.79
8	0.82	6.94	1.00	0.01	9.60	18.37
9	0.40	3.21	0.16	0.00	7.61	11.37
10	0.26	1.43	0.00	0.00	4.90	6.59
11	0.15	0.17	0.00	0.00	0.63	0.95
12	0.00	0.11	0.00	0.00	0.30	0.41
<u>Total</u>	<u>16.29</u>	<u>36.61</u>	<u>7.01</u>	<u>9.18</u>	<u>30.91</u>	<u>100.00</u>

Average Molecular Weight = 91.61

Average Density - .734

Average Carbon Number = 6.60

H/C Ratio = 1.86

TABLE 8. - Fuel composition summary - Rockville - winter

Volume-percent Summation by Carbon Number and Compound Class

Initial

Carbon No.	Paraffins		Naphthenes	Olefins	Aromatics	Total
	Normal	Iso				
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.19	0.00	0.00	0.03	0.00	0.22
4	7.41	1.77	0.00	2.54	0.00	11.72
5	7.00	10.49	0.18	4.80	0.00	22.48
6	2.47	8.54	1.66	3.64	1.21	17.52
7	1.22	5.72	2.07	1.40	5.70	15.11
8	0.52	7.65	1.59	0.07	7.04	16.87
9	0.35	3.01	0.08	0.00	6.41	9.87
10	0.25	0.83	0.00	0.00	3.69	4.77
11	0.11	0.03	0.00	0.00	0.29	0.43
12	0.00	0.01	0.00	0.00	0.03	0.03
Total	19.52	38.05	5.58	12.48	11.72	100.00

Average Molecular Weight = 88.15

Average Density = .716

Average Carbon Number = 6.31

H/C Ratio = 1.94

48 Hours

Carbon No.	Paraffins		Naphthenes	Olefins	Aromatics	Total
	Normal	Iso				
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.06	0.00	0.00	0.01	0.00	0.07
4	5.46	1.09	0.00	1.86	0.00	8.41
5	6.83	9.78	0.18	4.71	0.00	21.51
6	2.63	8.94	1.78	3.86	1.31	18.53
7	1.32	6.24	2.36	1.45	6.20	17.58
8	0.59	9.12	0.98	0.06	7.52	18.27
9	0.38	2.73	0.09	0.00	6.72	9.92
10	0.24	1.01	0.00	0.00	4.00	5.25
11	0.11	0.03	0.00	0.00	0.32	0.47
12	0.00	0.00	0.00	0.00	0.00	0.00
Total	17.42	38.94	5.39	11.95	26.07	99.72

Average Molecular Weight = 90.25

Average Density = .724

Average Carbon Number = 6.47

H/C Ratio = 1.91

TABLE 9. - Fuel composition summary - Sacramento - winter

Carbon No.	Volume-percent Summation by Carbon Number and Compound Class					Initial
	Normal	Paraffins Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.24	0.00	0.00	0.00	0.00	0.24
4	5.93	2.87	0.00	0.97	0.00	9.77
5	5.75	13.15	0.22	3.34	0.00	22.46
6	2.75	10.84	3.81	3.37	1.64	22.42
7	1.12	5.51	3.10	1.28	6.00	17.00
8	0.38	7.09	1.90	0.06	7.80	17.22
9	0.21	3.01	0.07	0.00	4.95	8.23
10	0.09	0.36	0.00	0.00	2.06	2.50
11	0.00	0.00	0.00	0.00	0.15	0.15
12	0.00	0.00	0.00	0.00	0.00	0.00
Total	16.46	42.84	9.10	9.01	22.59	100.00

Average Molecular Weight = 87.54

Average Density - .714

Average Carbon Number = 6.26

H/C Ratio = 1.96

Carbon No.	48 Hours					Total
	Normal	Paraffins Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.12	0.00	0.00	0.00	0.00	0.12
4	5.00	2.17	0.00	0.82	0.00	7.99
5	5.71	12.67	0.23	3.32	0.00	21.92
6	2.87	11.15	3.96	3.24	1.70	22.92
7	1.18	5.67	1.61	2.82	6.25	17.53
8	0.35	8.55	1.26	0.03	8.12	18.31
9	0.11	3.02	0.07	0.00	5.22	8.42
10	0.00	0.41	0.00	0.00	2.23	2.65
11	0.00	0.00	0.00	0.00	0.14	0.14
12	0.00	0.00	0.00	0.00	0.00	0.00
Total	15.33	43.65	7.13	10.24	23.65	100.00

Average Molecular Weight = 88.71

Average Density - .718

Average Carbon Number = 6.35

H/C Ratio = 1.94

TABLE 10. - Fuel composition summary - Houston

One-percent Summation by Carbon Number and Composition

Initial

<u>Carbon No.</u>	<u>Normal</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	<u>Total</u>
		<u>Iso</u>				
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.04	0.00	0.00	0.00	0.00	0.12
4	0.11	1.43	0.00	2.47	0.00	11.37
5	5.98	11.01	0.18	4.13	0.00	22.31
6	0.02	5.10	1.88	2.79	0.88	15.67
7	0.08	5.13	2.30	0.87	0.35	14.34
8	0.09	4.17	0.95	0.13	0.11	15.17
9	0.46	2.71	0.07	0.02	0.12	3.65
10	0.27	0.43	0.00	0.00	0.07	0.79
11	0.03	0.01	0.00	0.00	0.01	1.20
12	0.02	0.02	0.00	0.00	0.03	0.21
Total	100.00	—	5.34	9.7	21.57	100.00

Average Molecular weight = 89.95

Average density = .730

Average Carbon Number = 5.48

Octane = 0.92

48 Hours

<u>Carbon No.</u>	<u>Normal</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	<u>Total</u>
		<u>Iso</u>				
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.02	0.00	0.00	0.11	0.00	0.35
4	0.53	1.03	0.00	1.50	0.00	9.17
5	5.55	10.53	0.18	4.01	0.00	21.58
6	0.10	8.32	1.96	2.78	0.90	16.06
7	0.05	5.23	1.25	1.98	5.23	14.85
8	0.53	4.94	1.18	0.02	10.27	17.03
9	0.24	2.44	0.09	0.00	9.90	12.67
10	0.14	0.65	0.00	0.00	6.31	7.11
11	0.13	0.00	0.00	0.00	1.09	1.28
12	0.02	0.00	0.00	0.00	0.07	0.20
Total	100.00	33.16	4.66	10.30	33.78	100.00

Average Molecular weight = 91.54

Average density = .736

Average Carbon Number = 6.60

Octane = 0.91

TABLE 11. - Fuel composition summary - Wichita - winter

Carbon No.	<u>Initial</u>					Total
	Normal	Paraffins Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.12	0.00	0.00	0.00	0.00	0.12
4	11.92	1.45	0.00	2.73	0.00	16.11
5	6.22	7.29	0.16	3.92	0.00	17.59
6	3.56	7.03	2.06	3.34	1.21	17.20
7	1.56	8.90	1.49	1.28	5.44	18.66
8	0.56	9.20	1.10	0.08	7.29	18.22
9	0.29	2.45	0.00	0.00	5.33	8.07
10	0.15	0.86	0.00	0.00	2.76	3.77
11	0.04	0.00	0.00	0.00	0.22	0.26
12	0.00	0.00	0.00	0.00	0.00	0.00
Total	24.42	37.18	4.80	11.35	22.26	100.00

Average Molecular Weight = 87.02

Average Density - .710

Average Carbon Number = 6.22

H/C Ratio = 1.97

Carbon No.	<u>48 Hours</u>					Total
	Normal	Paraffins Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.04	0.00	0.00	0.00	0.00	0.04
4	9.04	0.94	0.00	2.06	0.00	12.04
5	6.04	6.79	0.17	3.80	0.00	16.81
6	3.73	7.29	2.16	3.50	1.25	17.93
7	1.67	9.58	1.58	1.35	5.87	20.06
8	0.60	10.00	1.21	0.10	7.82	19.72
9	0.33	2.81	0.01	0.00	5.81	8.94
10	0.15	0.73	0.00	0.00	3.18	4.06
11	0.05	0.00	0.00	0.00	0.35	0.41
12	0.00	0.00	0.00	0.00	0.00	0.00
Total	21.65	38.13	5.12	10.81	24.28	100.00

Average Molecular Weight = 89.57

Average Density - .719

Average Carbon Number = 6.41

H/C Ratio = 1.94

TABLE 12. - Fuel composition summary - Denver - winter

Volume-percent Summation by Carbon Number and Compound Class

Initial

<u>Carbon No.</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	<u>Total</u>
	<u>Normal</u>	<u>Iso</u>			
1	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00
3	0.25	0.00	0.00	0.00	0.26
4	5.23	5.73	0.00	2.54	0.00
5	6.84	8.49	0.19	1.53	0.00
6	5.48	9.02	3.84	2.55	1.28
7	3.25	5.97	3.08	1.63	0.32
8	0.67	3.91	0.71	0.07	1.64
9	0.37	2.27	0.02	0.00	0.73
10	0.19	0.39	0.00	0.00	0.23
11	0.14	0.00	0.00	0.00	0.38
12	0.00	0.00	0.00	0.00	0.00
Total	21.43	35.78	7.64	10.38	24.58
					100.00

Average Molecular Weight = 86.83

Average Density = .715

Average Carbon Number = 6.22

H/C Ratio = 1.94

48 Hours

<u>Carbon No.</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	<u>Total</u>
	<u>Normal</u>	<u>Iso</u>			
1	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00
3	0.07	0.00	0.00	0.00	0.07
4	3.87	3.48	0.00	1.85	0.00
5	6.63	7.88	0.19	3.39	0.00
6	5.79	9.33	4.05	2.65	1.35
7	2.44	6.90	2.91	1.80	6.85
8	0.76	4.24	0.82	0.10	8.37
9	0.41	2.52	0.01	0.00	6.24
10	0.21	0.47	0.00	0.00	3.66
11	0.13	0.00	0.00	0.00	0.62
12	0.00	0.00	0.00	0.00	0.00
Total	20.31	34.82	7.98	9.80	27.09
					100.00

Average Molecular Weight = 89.57

Average Density = .726

Average Carbon Number = 6.43

H/C Ratio = 1.96

TABLE 13. - Vapor pressure versus time - summer fuels

Fuel	Original	Equivalent Reid Vapor Pressure (psi)			
		0	12	24	48
New Orleans, LA	11.2	9.5	9.3	9.2	9.2
Houston, TX	8.8	8.2	7.6	7.7	7.4
Washington, DC	9.9	9.7	8.5	8.4	8.2
Denver, CO	9.2	8.9	8.4	8.5	8.3
Ft. Lauderdale, FL	10.6	9.8	9.5	9.3	9.3
Chicago, IL	10.2	9.6	9.5	9.3	9.3
Sacramento, CA	8.7	8.4	8.3	8.2	8.0
San Diego, CA	8.9	8.4	8.2	8.2	8.1
Wichita, KS	8.9	8.8	8.6	8.4	8.4
Duluth, MN	10.6	9.3	8.3	7.9	8.1

TABLE 14. - Octane ratings - summer fuels

Fuel	RON			MON		
	Initial	Final	Diff.	Initial	Final	Diff.
New Orleans, LA	95.2	95.1	0.1	83.7	83.7	0.0
Houston, TX	97.5	97.5	0.0	86.5	86.5	0.0
Washington, DC	91.7	91.4	0.3	81.6	81.6	0.0
Denver, CO	89.4	89.4	0.0	80.1	80.0	0.0
Ft. Lauderdale, FL	97.5	97.5	0.0	86.8	86.8	0.0
Chicago, IL	93.1	93.0	0.1	83.7	83.7	0.0
Sacramento, CA	98.1	97.5	0.6	85.8	85.0	0.8
San Diego, CA	92.7	92.6	0.1	82.2	82.2	0.0
Wichita, KS	94.1	94.0	0.1	85.0	84.8	0.2
Duluth, MN	94.9	94.0	0.0	86.4	86.1	0.3

DISTILLATION (%)

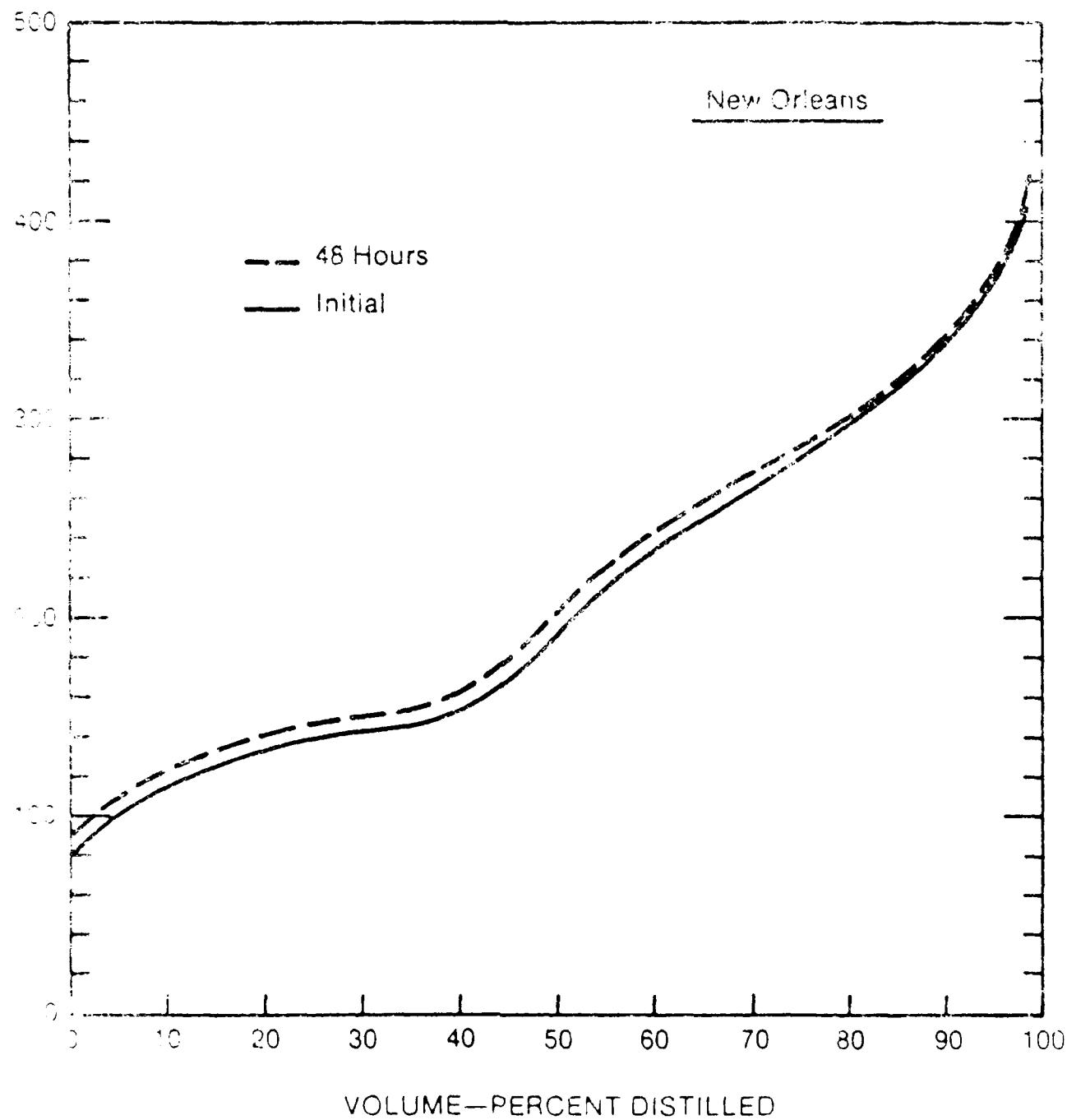


FIGURE 15. - Changes in distillation character due to weathering,
summer fuel from New Orleans

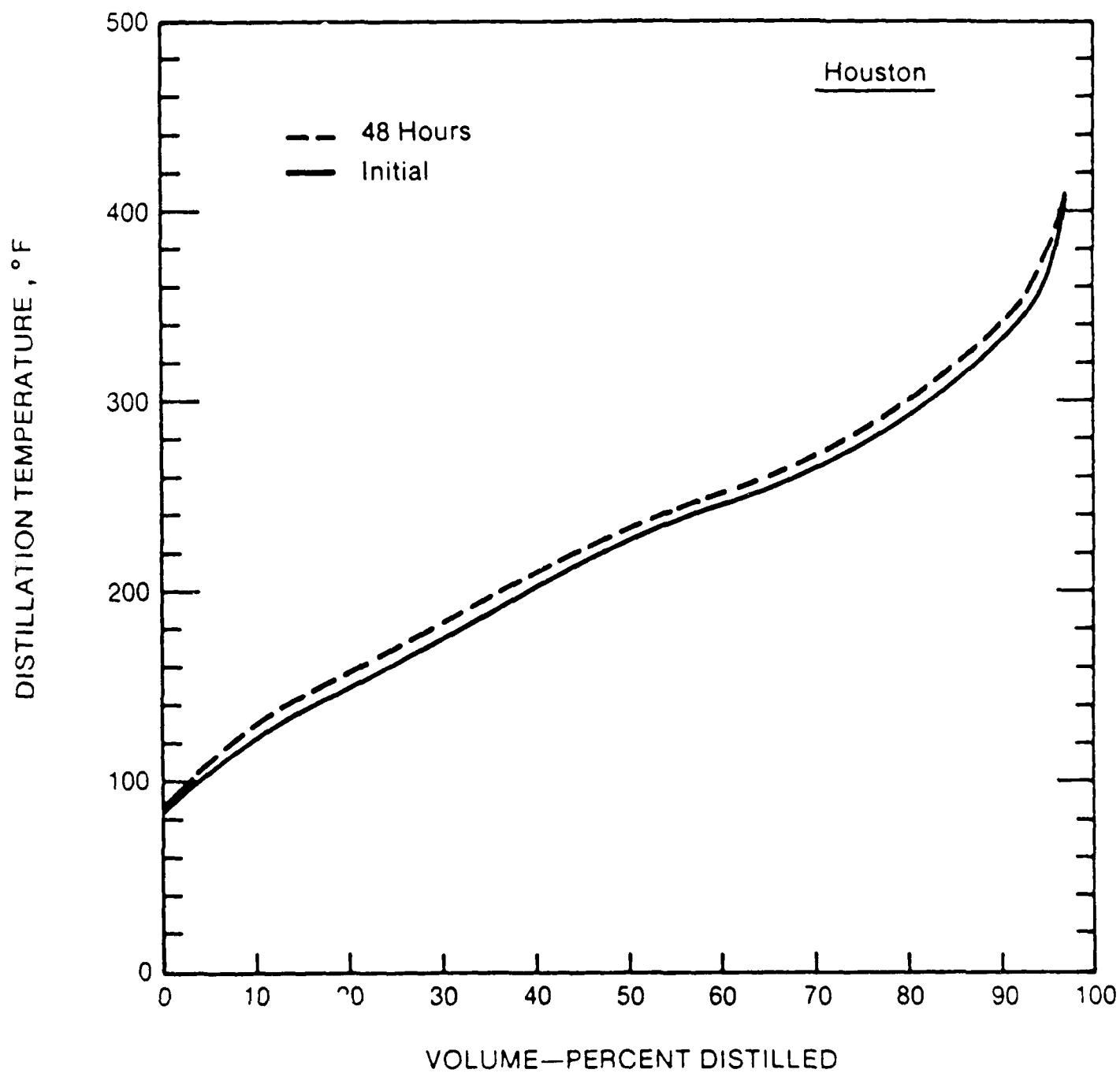


FIGURE 17. - Changes in distillation character due to weathering, summer fuels from Houston.

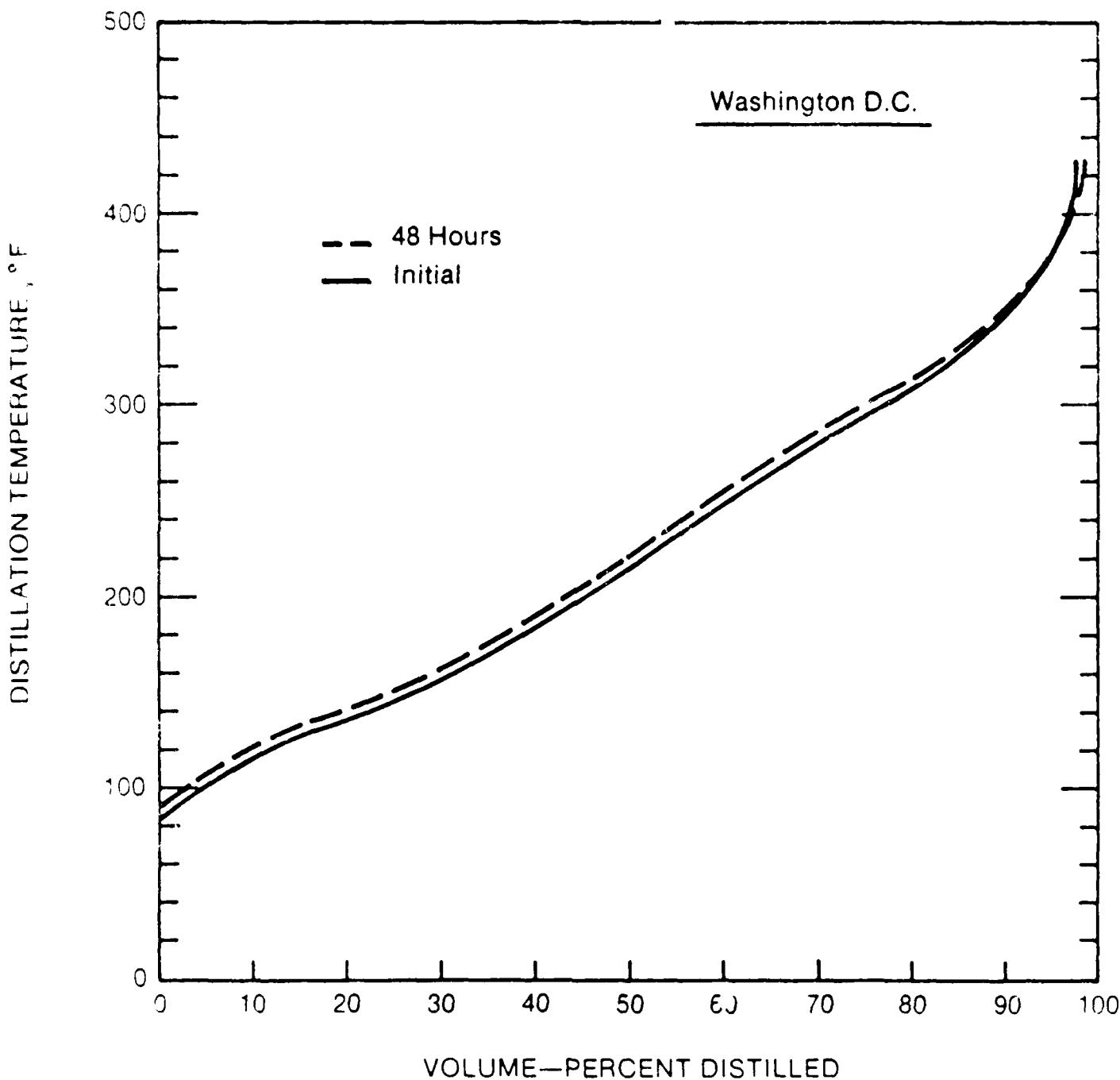


FIGURE 18. - Changes in distillation character due to weathering,
summer fuels from Washington, DC

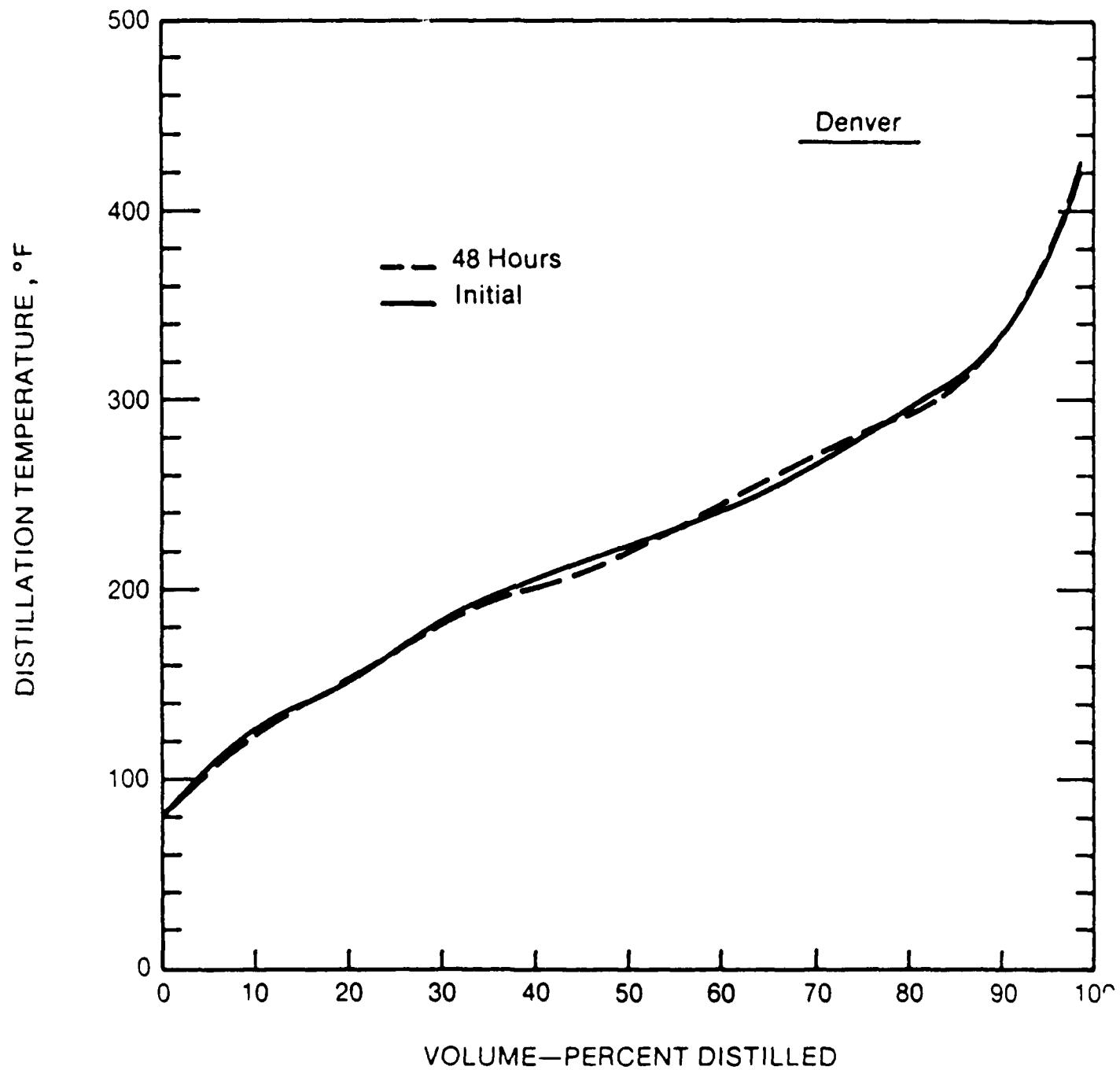


FIGURE 19. - Changes in distillation character due to weathering, summer fuel from Denver.

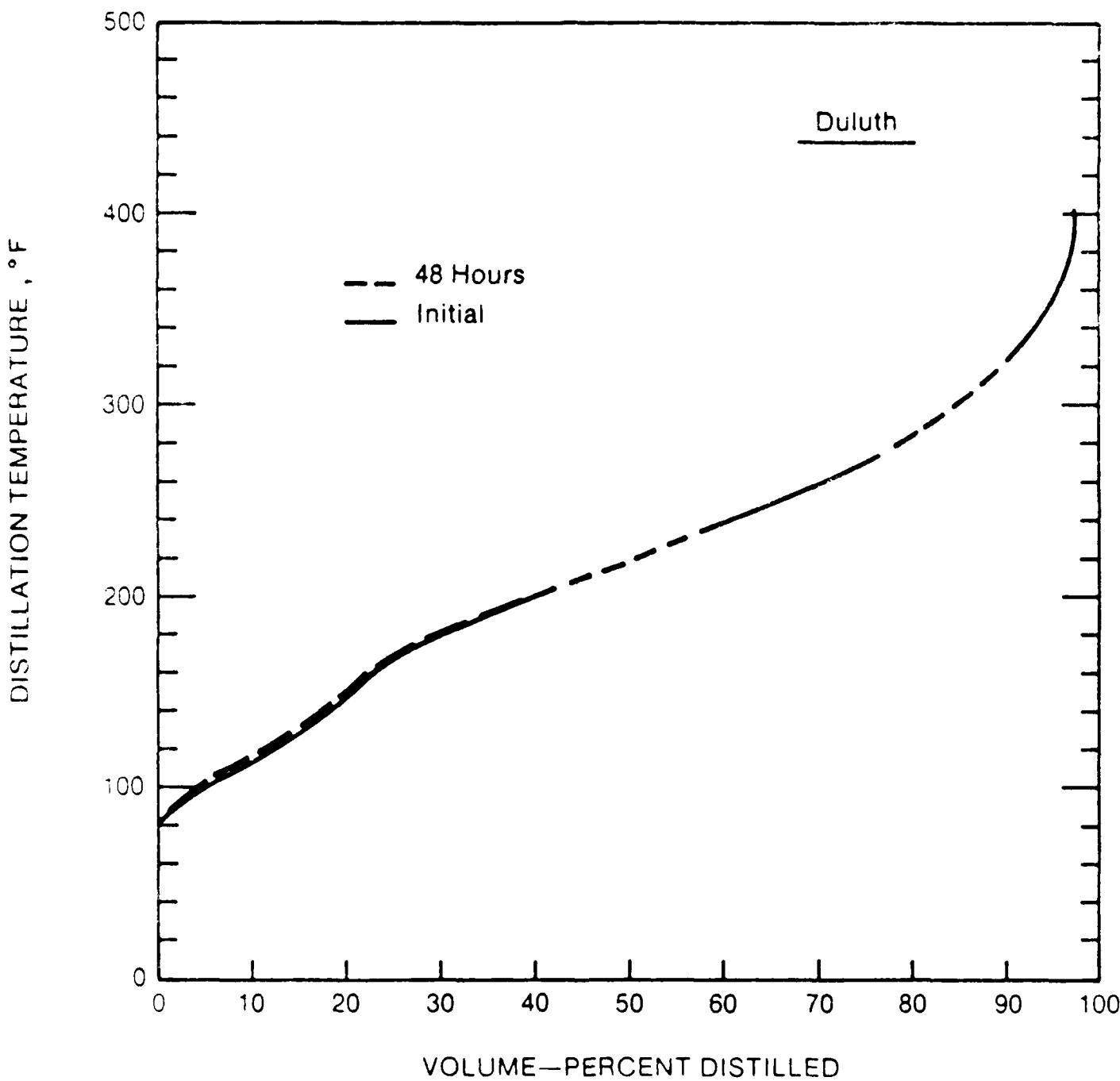


FIGURE 20. - Changes in distillation character due to weathering, summer fuel from Duluth.

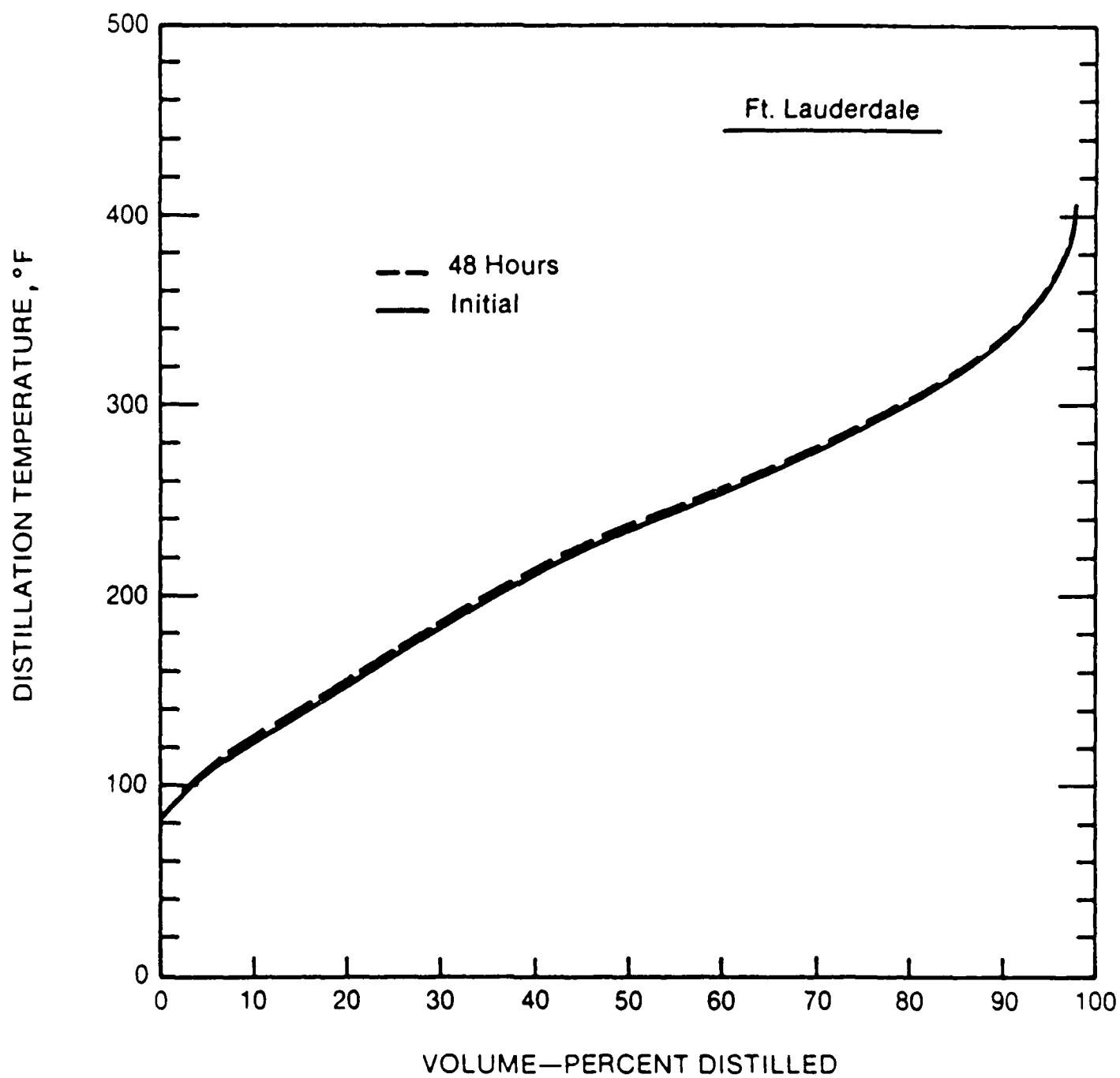


FIGURE 21. - Changes in distillation character due to weathering,
summer fuel from Ft. Lauderdale.

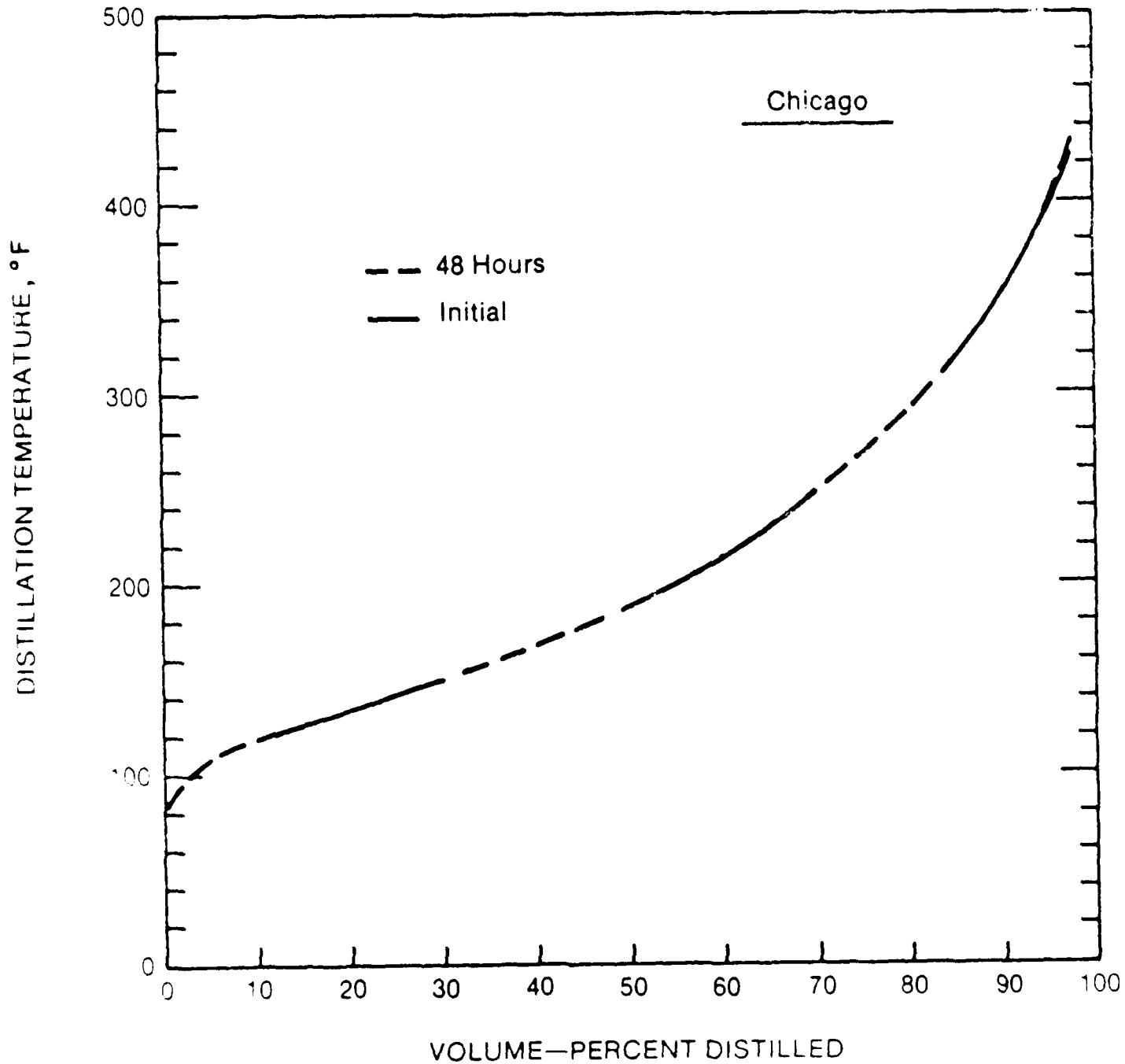


FIGURE 22. - Changes in distillation character due to weathering, summer fuel from Chicago.

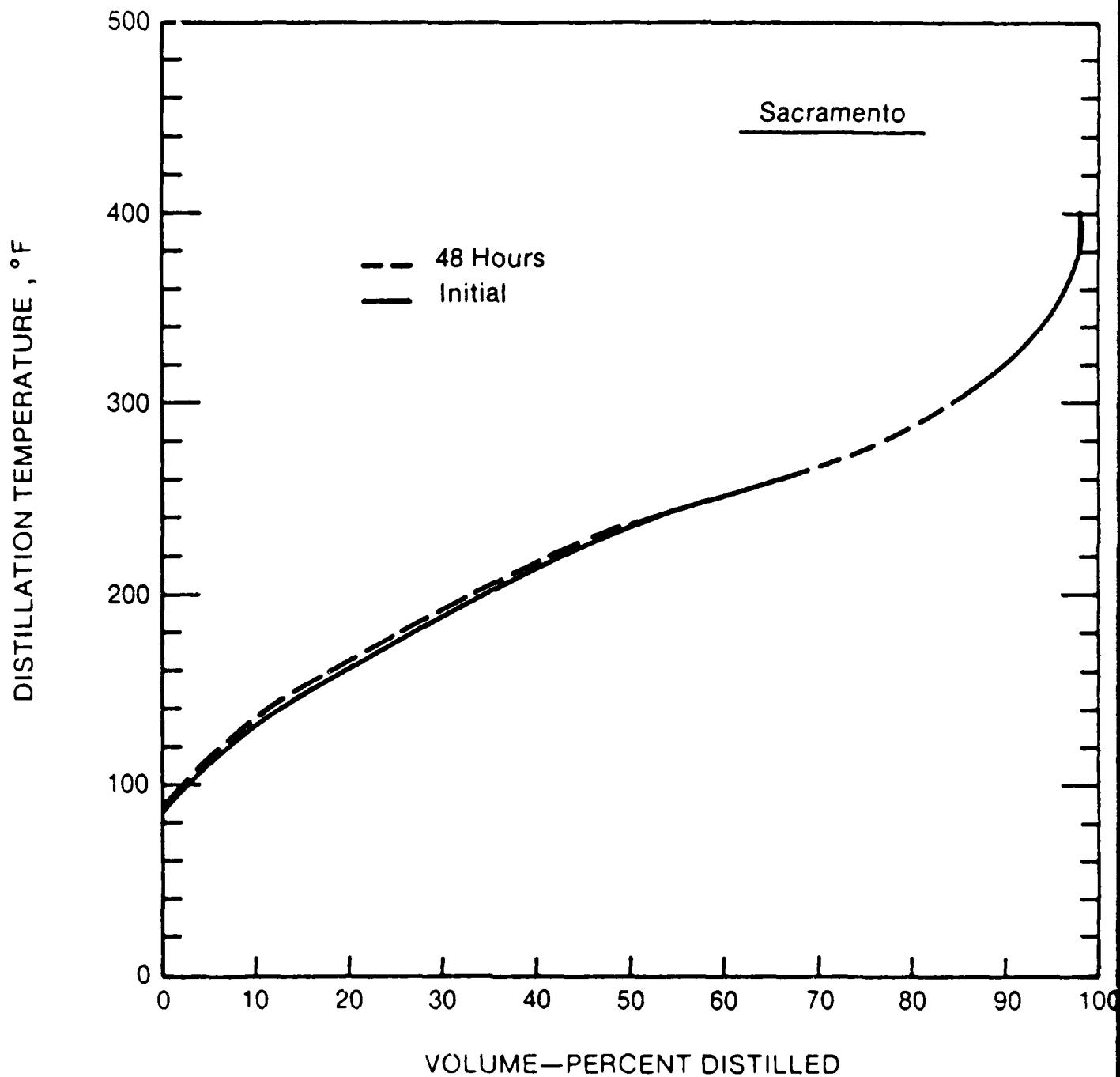


FIGURE 23. - Changes in distillation character due to weathering,
summer fuel from Sacramento

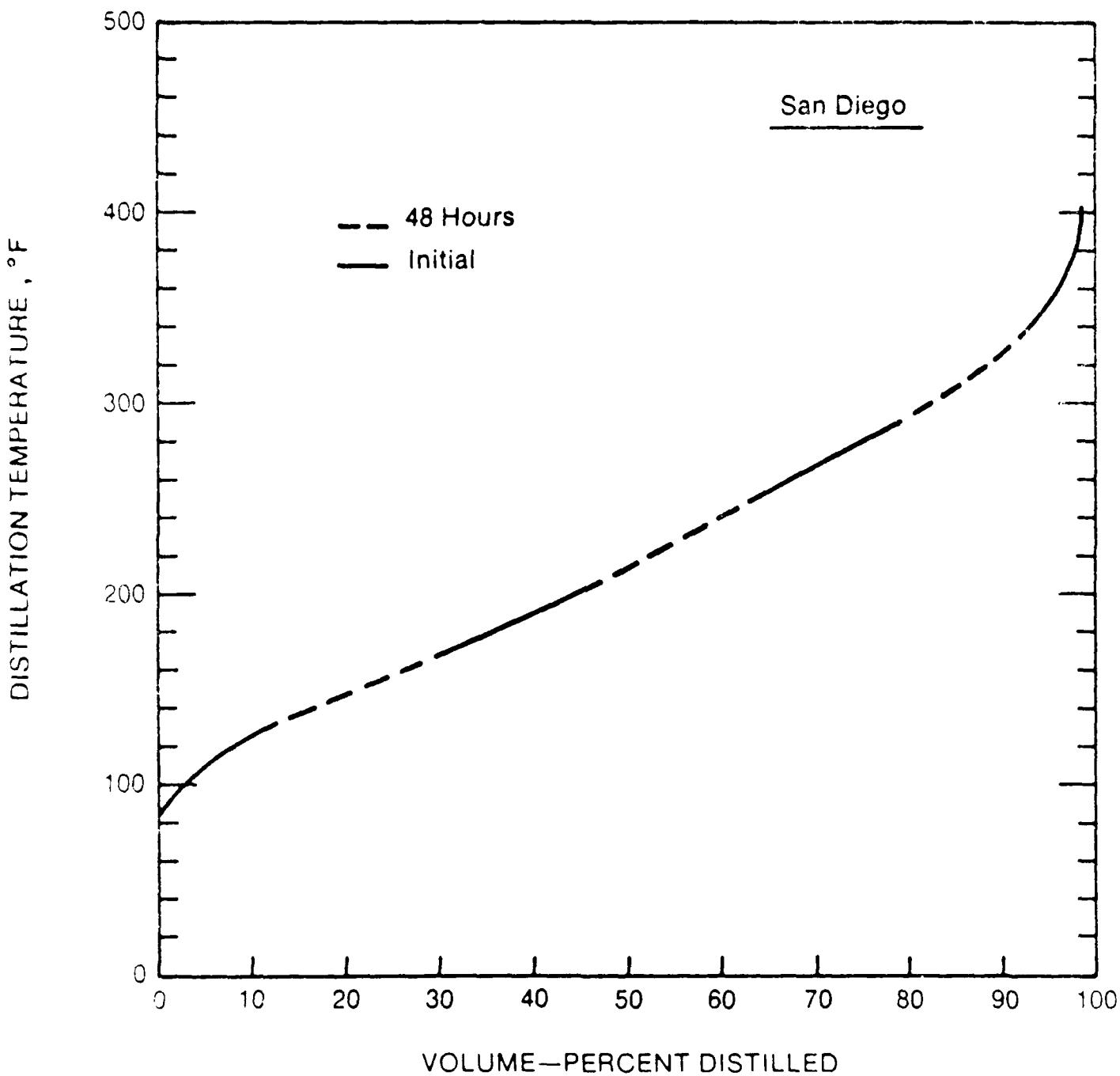


FIGURE 24. - Changes in distillation character due to weathering, summer fuel from San Diego.

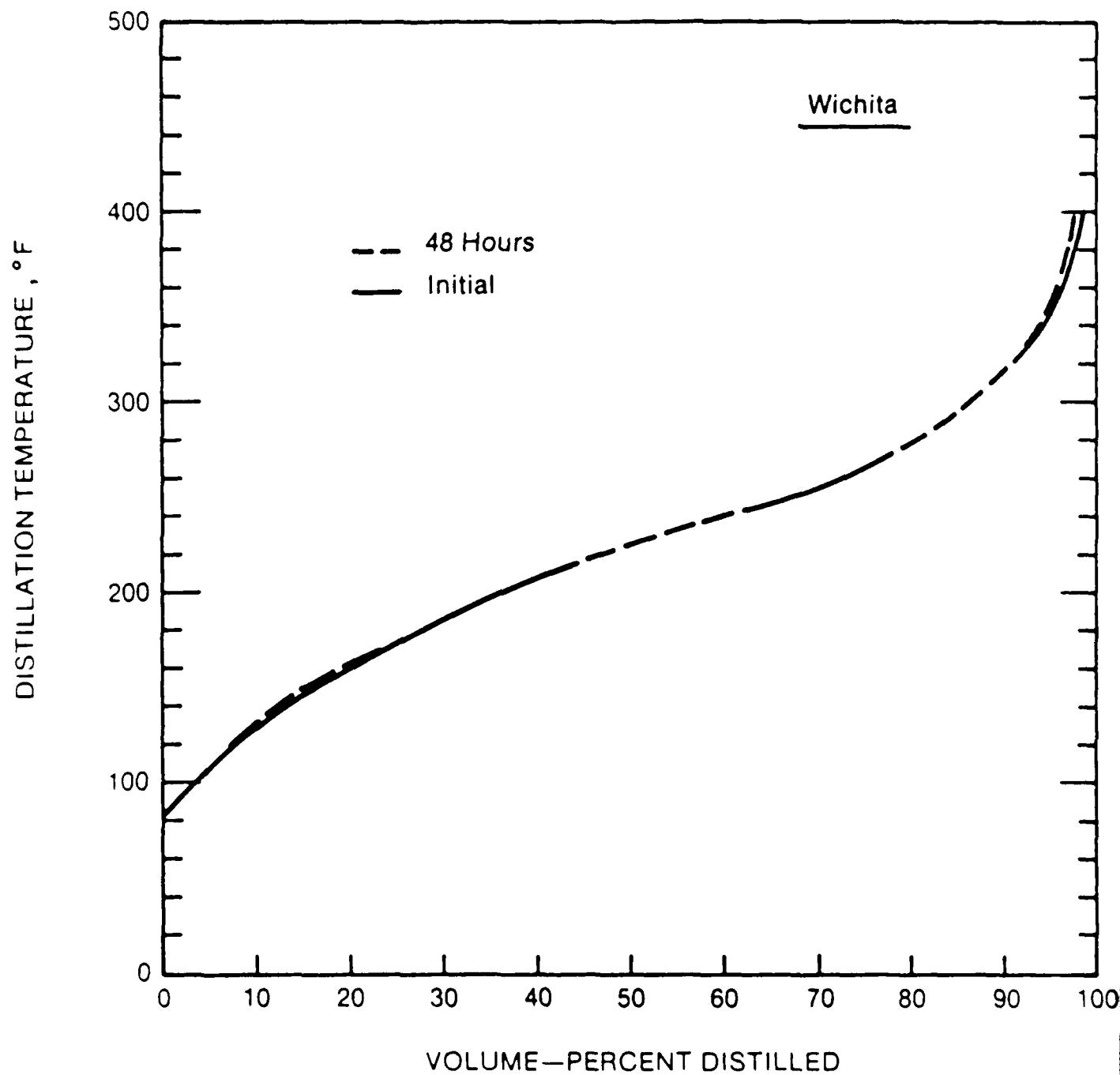


FIGURE 25. - Changes in distillation character due to weathering,
summer fuel from Wichita.

TABLE 15. - Fuel composition summary - Denver - summer

Volume-percent Summation by Carbon Number and Compound Class

Initial

Carbon No.	Paraffins		Naphthenes	Olefins	Aromatics	Total
	Normal	Iso				
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.46	0.00	0.00	0.02	0.00	0.48
4	2.77	1.54	0.00	1.58	0.00	5.89
5	6.20	7.89	0.17	3.25	0.00	17.52
6	4.68	7.18	3.13	4.01	1.48	20.48
7	2.40	6.29	1.64	3.22	7.78	21.33
8	0.92	5.48	1.06	0.46	9.14	17.07
9	0.24	3.08	0.09	0.00	7.30	10.72
10	0.13	0.87	0.00	0.00	4.46	5.47
11	0.08	0.20	0.00	0.00	0.63	0.91
12	0.00	0.13	0.00	0.00	0.00	0.13
Total	17.89	32.67	6.10	12.54	30.80	100.00

Average Molecular Weight = 92.23

Average Density = .736

Average Carbon Number = 6.64

H/C Ratio = 1.85

48 Hours

Carbon No.	Paraffins		Naphthenes	Olefins	Aromatics	Total
	Normal	Iso				
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.24	0.00	0.00	0.11	0.00	0.35
4	8.91	1.94	0.00	1.11	0.00	11.96
5	3.90	5.09	0.12	2.04	0.00	11.15
6	3.91	5.89	2.73	3.26	1.19	16.97
7	2.34	6.03	1.62	3.39	7.92	21.30
8	1.00	5.53	1.25	0.38	10.35	18.52
9	0.27	3.45	0.09	0.00	8.57	12.38
10	0.14	0.93	0.00	0.00	5.15	6.23
11	0.09	0.21	0.00	0.00	0.71	1.02
12	0.00	0.13	0.00	0.00	0.00	0.13
Total	20.30	29.19	5.82	10.29	33.89	100.00

Average Molecular Weight = 92.41

Average Density = .740

Average Carbon Number = 6.19

H/C Ratio = 1.83

TABLE 16. - Fuel composition summary - Wichita - summer

Carbon No.	<u>Initial</u>					<u>Total</u>
	<u>Normal</u>	<u>Paraffins</u> <u>Iso</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.11	0.00	0.00	0.07	0.00	0.17
4	6.48	1.05	0.00	1.79	0.00	9.33
5	2.72	5.94	0.08	2.57	0.00	11.32
6	2.27	5.41	0.87	3.19	1.41	13.15
7	1.49	7.27	1.72	2.56	6.85	19.90
8	0.49	19.98	0.91	0.38	9.33	31.08
9	0.12	4.23	0.20	0.00	5.81	10.35
10	0.04	1.56	0.00	0.00	2.88	4.48
11	0.02	0.01	0.00	0.00	0.20	0.23
12	0.00	0.00	0.00	0.00	0.00	0.00
<u>Total</u>	<u>13.75</u>	<u>45.44</u>	<u>3.77</u>	<u>10.57</u>	<u>26.48</u>	<u>100.00</u>

Average Molecular Weight = 94.48

Average Density = .730

Average Carbon Number = 6.78

H/C Ratio = 1.91

Carbon No.	<u>48 Hours</u>					<u>Total</u>
	<u>Normal</u>	<u>Paraffins</u> <u>Iso</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.08	0.00	0.00	0.04	0.00	0.13
4	7.55	1.21	0.00	1.57	0.00	10.33
5	1.41	3.22	0.05	1.28	0.00	5.96
6	2.20	4.15	0.73	1.99	1.04	10.12
7	1.49	6.78	1.53	2.33	6.92	19.04
8	0.59	21.42	1.10	0.34	11.37	34.83
9	0.16	5.10	0.25	0.00	7.81	13.31
10	0.05	2.24	0.00	0.00	3.68	5.97
11	0.03	0.02	0.00	0.00	0.27	0.32
12	0.00	0.00	0.00	0.00	0.00	0.00
<u>Total</u>	<u>13.56</u>	<u>44.14</u>	<u>3.66</u>	<u>7.56</u>	<u>31.08</u>	<u>100.00</u>

Average Molecular Weight = 97.65

Average Density = .741

Average Carbon Number = 6.62

H/C Ratio = 1.87

TABLE 17. - Fuel composition summary - Washington DC - 1958

Volume-percent Summation by Carbon Number and Component

Initial

<u>Carbon No.</u>	<u>Normal</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	<u>Total</u>
		<u>Iso</u>				
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.61	0.00	0.00	0.08	0.00	0.68
4	0.72	2.47	0.00	2.06	0.00	12.26
5	4.69	8.99	0.16	4.42	0.00	18.26
6	2.83	7.15	1.78	4.22	1.43	17.41
7	1.46	4.96	1.68	2.51	5.22	16.40
8	0.54	8.83	0.85	0.20	8.56	18.49
9	0.18	2.74	0.07	0.00	7.16	10.00
10	0.12	0.83	0.00	0.00	4.40	5.42
11	0.12	0.18	0.00	0.00	0.38	0.88
12	0.06	0.08	0.00	0.00	0.00	0.14
Total	10.00	36.23	4.54	13.49	27.41	100.00

Average Molecular Weight = 89.26

Average Density = .722

Average Carbon Number = 6.15

H/C Ratio = 1.90

48 Hours

<u>Carbon No.</u>	<u>Normal</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	<u>Total</u>
		<u>Iso</u>				
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.57	0.00	0.00	1.05	0.00	0.61
4	1.36	2.34	0.00	1.89	0.00	11.59
5	3.64	8.87	0.16	4.37	0.00	18.04
6	1.37	7.19	1.78	4.27	1.43	17.53
7	1.17	5.01	1.69	2.52	5.90	16.60
8	0.59	3.95	0.90	0.21	8.24	18.88
9	0.11	2.81	0.08	0.00	7.24	10.32
10	0.10	0.90	0.00	0.00	4.40	5.41
11	0.13	0.13	0.00	0.00	0.55	0.86
12	0.07	0.08	0.00	0.00	0.00	0.15
Total	10.00	36.34	4.61	13.30	27.75	100.00

Average Molecular weight = 89.76

Average Density = .722

Average Carbon Number = 6.20

TABLE 18. - Fuel composition summary - San Diego - summer

Carbon No.	Volume-percent Summation by Carbon Number and Compound Class					<u>Initial</u>
	Normal	Paraffins Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.28	0.00	0.00	0.08	0.00	0.36
4	15.37	2.61	0.00	3.61	0.00	21.59
5	3.67	10.72	0.13	3.34	0.00	17.85
6	2.37	7.80	2.98	3.81	1.28	18.25
7	1.15	4.79	1.87	2.45	5.67	15.93
8	0.43	3.71	0.99	0.09	8.06	13.28
9	0.12	2.02	0.05	0.00	6.36	8.55
10	0.06	0.19	0.00	0.00	3.28	3.53
11	0.00	0.02	0.00	0.00	0.18	0.20
12	0.00	0.48	0.00	0.00	0.00	0.48
Total	23.47	32.32	6.02	13.37	24.82	100.00

Average Molecular Weight = 83.84

Average Density = .707

Average Carbon Number = 5.13

H/C Ratio = 1.94

Carbon No.	48 Hours					<u>Initial</u>
	Normal	Paraffins Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.15	0.00	0.00	0.05	0.00	0.20
4	7.15	1.30	0.00	2.09	0.00	10.54
5	2.97	11.39	0.15	4.62	0.00	19.13
6	2.32	8.63	3.36	4.53	1.48	20.32
7	1.30	5.55	2.13	2.79	6.43	18.20
8	0.53	4.33	1.38	0.21	9.23	15.67
9	0.14	2.35	0.08	0.00	7.44	10.02
10	0.08	0.50	0.00	0.00	4.20	4.78
11	0.06	0.16	0.00	0.00	0.65	0.87
12	0.00	0.23	0.00	0.00	0.05	0.28
Total	14.71	34.43	7.09	14.28	29.49	100.00

Average Molecular Weight = 89.32

Average Density = .729

Average Carbon Number = 6.08

H/C Ratio = 1.97

TABLE 19. - Fuel composition summary - Rovcor - 100%
Volume-percent summation by Carbon Number and Catalyst

Carbon No.	<u>Initial</u>					Total
	Normal	Iso	Naphthenes	Olefins	Aromatics	
1.00	0.00	0.00	0.00	0.00	0.00	0.00
2.00	0.00	0.00	0.00	0.00	0.00	0.00
3.00	0.00	0.00	0.00	0.00	0.00	0.10
4.00	0.88	0.00	0.00	2.36	0.00	8.91
5.00	7.93	0.11	4.64	0.00	15.69	
6.00	5.61	1.31	2.85	1.20	12.45	
7.00	4.29	0.91	1.47	9.32	17.21	
8.00	15.41	0.44	0.10	12.24	19.53	
9.00	1.95	0.00	0.00	0.56	11.12	
10.00	0.22	0.00	0.00	0.19	4.59	
11.00	0.00	0.00	0.00	0.01	0.53	
12.00	0.31	0.00	0.00	0.00	0.31	
Total	36.59	2.75	11.46	35.81	100.00	

Average Molecular Weight = 93.15

Average Density = 742

Average Carbon Number = 6.74

Catalyst = 1.79

48 Hours

Carbon No.	<u>48 Hours</u>					Total
	Normal	Iso	Naphthenes	Olefins	Aromatics	
1.00	0.00	0.00	0.00	0.00	0.00	0.00
2.00	0.00	0.00	0.00	0.00	0.00	0.00
3.00	0.00	0.00	0.00	0.04	0.00	0.57
4.00	2.36	0.00	2.19	0.00	12.50	
5.00	7.33	0.10	4.49	0.00	14.73	
6.00	5.30	1.43	2.77	1.14	12.42	
7.00	4.14	1.05	1.17	9.27	16.68	
8.00	14.63	0.45	0.02	11.99	27.44	
9.00	1.88	0.00	0.00	8.54	10.62	
10.00	0.14	0.00	0.00	4.04	4.26	
11.00	0.00	0.00	0.00	0.45	0.45	
12.00	0.33	0.00	0.00	0.00	0.33	
Total	36.12	3.03	10.68	35.43	100.00	

Average Molecular Weight = 91.07

Average Density = 740

Average Carbon Number = 6.32

Catalyst = 1.79

TABLE 20. - Fuel composition summary - Sacramento - summer

Carbon No.	Initial					<u>Total</u>
	<u>Normal</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.27	0.00	0.00	0.08	0.00	0.35
4	8.72	1.88	0.00	1.08	0.00	11.68
5	1.70	4.80	0.09	2.04	0.00	8.63
6	2.20	5.63	1.41	2.97	2.84	14.85
7	1.57	5.02	0.92	1.87	12.68	22.06
8	0.57	5.43	0.38	0.11	17.06	23.54
9	0.23	1.44	0.00	0.00	11.73	13.40
10	0.09	0.18	0.00	0.00	4.66	4.92
11	0.00	0.00	0.00	0.00	0.55	0.55
12	0.00	0.00	0.00	0.00	0.00	0.00
Total	15.35	24.37	2.60	8.16	49.52	100.00

Average Molecular Weight = 93.00

Average Density = .766

Average Carbon Number = 6.34

H/C Ratio = 1.67

Carbon No.	<u>48 Hours</u>					<u>Total</u>
	<u>Normal</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.24	0.00	0.00	0.10	0.00	0.33
4	8.68	1.82	0.00	1.06	0.00	11.56
5	1.71	4.71	0.09	2.07	0.00	8.57
6	2.16	5.65	1.23	3.05	2.92	15.02
7	1.57	5.04	0.93	1.88	12.80	22.22
8	0.57	5.45	0.38	0.11	16.94	23.45
9	0.23	1.35	0.00	0.00	11.72	13.30
10	0.09	0.13	0.00	0.00	4.71	4.93
11	0.00	0.05	0.00	0.00	0.56	0.62
12	0.00	0.00	0.00	0.00	0.00	0.00
Total	15.24	24.21	2.63	8.27	49.65	100.00

Average Molecular Weight = 93.04

Average Density = .766

Average Carbon Number = 6.34

H/C Ratio = 1.66

TABLE 21. - Fuel composition summary - Fort Lauderdale - summer

Volume-percent Summation by Carbon Number and Compound Class

Initial

<u>Carbon No.</u>	<u>Normal</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	<u>Total</u>
		<u>Iso</u>				
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.50	0.00	0.00	0.07	0.00	0.57
4	7.85	2.58	0.00	1.67	0.00	12.10
5	5.38	7.40	0.16	3.28	0.00	16.22
6	1.26	4.03	0.63	1.82	0.93	8.67
7	1.12	3.77	0.88	0.99	11.09	17.85
8	3.55	14.80	0.24	0.10	11.52	27.22
9	0.18	1.41	0.00	0.00	8.90	10.49
10	0.08	0.47	0.00	0.00	5.04	5.59
11	0.00	0.46	0.00	0.00	0.62	1.08
12	0.00	0.22	0.00	0.00	0.00	0.22
Total	16.93	35.12	1.92	7.94	38.10	100.00

Average Molecular Weight = 91.95

Average Density = .743

Average Carbon Number = 6.42

H/C Ratio = 1.79

48 Hours

<u>Carbon No.</u>	<u>Normal</u>	<u>Paraffins</u>	<u>Naphthenes</u>	<u>Olefins</u>	<u>Aromatics</u>	<u>Total</u>
		<u>Iso</u>				
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.12	0.00	0.00	0.08	0.00	0.20
4	3.25	1.42	0.00	0.68	0.00	10.35
5	2.79	3.91	0.10	2.12	0.00	8.92
6	1.07	3.15	0.60	2.16	0.77	7.75
7	1.19	3.34	0.59	0.72	12.13	17.98
8	0.67	16.82	0.31	0.11	14.33	32.24
9	0.24	1.76	0.00	0.00	11.64	13.64
10	0.10	0.61	0.00	0.00	6.60	7.30
11	0.01	0.65	0.00	0.00	0.80	1.47
12	0.00	0.17	0.00	0.00	0.00	0.17
Total	14.43	31.83	1.60	5.88	46.26	100.00

Average Molecular Weight = 97.01

Average Density = .76

Average Carbon Number = 6.64

TABLE 22. - Fuel composition summary - Duluth - summer

Carbon No.	Normal	Volume-percent Summation by Carbon Number and Compound Class					Initial
		Paraffins	Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3	0.63	0.00	0.00	0.04	0.00	0.00	0.67
4	9.86	3.71	0.00	2.19	0.00	0.00	15.76
5	2.60	5.94	0.05	1.34	0.00	0.00	9.94
6	2.27	5.81	0.88	2.09	2.20	0.00	13.24
7	1.29	6.79	1.44	1.66	8.09	0.00	19.28
8	0.41	18.28	0.25	0.06	9.04	0.00	28.06
9	0.09	1.68	0.00	0.00	6.17	0.00	7.95
10	0.04	1.00	0.00	0.00	3.61	0.00	4.65
11	0.02	0.19	0.00	0.00	0.25	0.00	0.47
12	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Total	17.21	43.40	2.63	7.39	29.36	0.00	100.00

Average Molecular Weight = 90.48

Average Density = .725

Average Carbon Number = 6.24

H/C Ratio = 1.89

Carbon No.	Normal	48 Hours					Total
		Paraffins	Iso	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3	0.08	0.00	0.00	0.04	0.00	0.00	0.12
4	7.07	1.32	0.00	1.24	0.00	0.00	9.63
5	1.28	2.95	0.04	0.69	0.00	0.00	4.95
6	2.03	4.51	0.81	1.52	1.68	0.00	10.56
7	1.44	7.14	1.43	1.68	8.98	0.00	20.68
8	0.56	21.29	0.36	0.07	12.14	0.00	34.41
9	0.14	2.34	0.00	0.00	9.14	0.00	11.61
10	0.06	1.56	0.00	0.00	5.44	0.00	7.06
11	0.04	0.09	0.00	0.00	0.77	0.00	0.90
12	0.00	0.08	0.00	0.00	0.00	0.00	0.08
Total	12.69	41.28	2.64	5.25	38.15	0.00	100.00

Average Molecular Weight = 98.22

Average Density = .754

Average Carbon Number = 6.73

H/C Ratio = 1.79

TABLE 23. - Fuel composition summary - New Orleans - summer

Carbon No.	<u>Initial</u>					Total
	Normal	Paraffins <u>Iso</u>	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.59	0.00	0.00	0.10	0.00	0.69
4	8.74	3.65	0.00	2.10	0.00	14.49
5	5.23	6.29	0.14	2.70	0.00	14.36
6	4.24	6.43	2.24	3.63	1.71	18.25
7	1.61	5.27	1.25	2.14	7.21	17.48
8	0.54	5.19	0.81	0.15	10.29	16.98
9	0.16	2.51	0.08	0.00	8.30	11.05
10	0.08	0.63	0.00	0.00	4.82	5.53
11	0.05	0.19	0.00	0.00	0.68	0.92
12	0.00	0.20	0.00	0.00	0.04	0.24
Total	21.24	30.37	4.51	10.83	33.06	100.00

Average Molecular Weight = 89.21

Average Density = .731

Average Carbon Number = 6.16

H/C Ratio = 1.84

48 Hours

Carbon No.	<u>48 Hours</u>					Total
	Normal	Paraffins <u>Iso</u>	Naphthenes	Olefins	Aromatics	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.54	0.00	0.00	0.08	0.00	0.63
4	6.91	3.15	0.00	2.15	0.00	12.21
5	5.37	5.93	0.14	2.72	0.00	14.16
6	4.29	6.48	2.27	3.64	1.74	18.42
7	1.66	5.40	1.40	2.15	7.50	18.11
8	0.57	5.26	0.85	0.15	10.75	17.58
9	0.16	2.74	0.08	0.00	8.64	11.62
10	0.28	0.55	0.00	0.00	5.30	6.13
11	0.05	0.19	0.00	0.00	0.67	0.91
12	0.00	0.19	0.00	0.00	0.04	0.23
Total	19.84	29.90	4.74	10.89	34.63	100.00

Average Molecular Weight = 90.64

Average Density = .737

Average Carbon Number = 6.27

H/C Ratio = 1.81

TABLE 24. - Fuel composition summary - Chicago - summer

Carbon No.	Initial					<u>Total</u>
	<u>Normal</u>	<u>Paraffins</u>	<u>Iso</u>	<u>Naphthenes</u>	<u>Olefins</u>	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.67	0.00	0.00	0.04	0.00	0.71
4	6.30	2.57	0.00	1.93	0.00	10.80
5	5.94	10.82	0.21	6.56	0.00	23.53
6	3.78	10.04	2.95	5.22	1.99	23.98
7	1.64	4.40	1.55	2.53	8.10	18.22
8	0.66	3.86	0.71	0.18	4.79	10.19
9	0.09	1.75	0.06	0.00	5.02	6.93
10	0.09	0.30	0.00	0.00	3.80	4.20
11	0.16	0.16	0.00	0.00	0.67	0.99
12	0.13	0.26	0.00	0.00	0.04	0.44
<u>Total</u>	<u>19.47</u>	<u>34.16</u>	<u>5.49</u>	<u>16.46</u>	<u>24.42</u>	<u>100.00</u>

Average Molecular Weight = 85.82

Average Density = .716

Average Carbon Number = 5.91

H/C Ratio = 1.91

Carbon No.	<u>48 Hours</u>					<u>Total</u>
	<u>Normal</u>	<u>Paraffins</u>	<u>Iso</u>	<u>Naphthenes</u>	<u>Olefins</u>	
1	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00
3	0.09	0.00	0.00	0.05	0.00	0.15
4	6.98	1.17	0.00	1.63	0.00	9.79
5	2.34	4.55	0.12	3.17	0.00	10.18
6	2.98	7.39	2.44	3.73	1.48	18.03
7	1.95	4.94	1.86	3.27	10.42	22.44
8	1.00	6.02	1.32	0.25	8.31	16.90
9	0.16	2.99	0.11	0.00	9.00	12.26
10	0.17	0.81	0.00	0.00	6.51	7.49
11	0.29	0.31	0.00	0.00	1.04	1.63
12	0.24	0.79	0.00	0.00	0.11	1.14
<u>Total</u>	<u>16.20</u>	<u>28.98</u>	<u>5.85</u>	<u>12.10</u>	<u>36.87</u>	<u>100.00</u>

Average Molecular Weight = 94.21

Average Density = .752

Average Carbon Number = 6.39

H/C Ratio = 1.78

APPENDIX A

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2701 Forum Drive
Grand Prairie, TX 75053-4005

Aviation International, Inc.
P.O. Box 117
Spokane, WA 99217

Avian Balloon Company
South 3722 Ridgeview Drive
Spokane, WA 99206

Aerojet General Corporation
Ninth and Red Lion Roads
Sacramento, CA 95854

Avtek Corporation
509 Calle Carga
Camarillo, CA 93010

McAllister Manufacturing, Incorporated
Route 1
Tulare, CA
Tulare, CA 93268

Avtek Corporation
509 Calle Carga
Camarillo, CA 93010

Avtek Corporation
P.O. Box 447
P.O. Box 374

Ayres Corporation
P.O. Box 3090
Municipal Airport
Albany, GA 31708

Autogyro Designs, Incorporated
1000 Franklin Court
Mountain View, CA 95014

Barnett Rotorcraft
4307 Olivehurst Avenue
Olivehurst, CA 95961

Aviation Supply Company
P.O. Box 1001
Atlanta, GA 30301

Barney Oldfield Aircraft
P.O. Box 228
Needham, MA 02192

Aviation, Incorporated
P.O. Box 1003
Pittsburgh, PA 15236

Beech Aircraft Corporation
Box 85
Wichita, KS 67201-0085

Aviation Company
P.O. Box 143
Tucson, AZ 85502

Bell Helicopter Textron
P.O. Box 482
Fort Worth, TX 76101

Aviation Corporation
Westgate Center
Charlotte-Wilmington Airport
Charlotte, NC 28262
Charlotte, NC 28262

Bellanca, Inc.
P.O. Box 964
Alexandria, MN 56308

Bensen Aircraft Corporation
P.O. Box 31047
Raleigh, NC 27622

CDX Aviation Sales
11343 104th Street
Edmonton, Alberta
TSG 2K7
CANADA

Boeing Commercial Airplane
Company
P.O. Box 3707
Seattle, WA 98124

Cessna Aircraft Company
P.O. Box 1521
Wichita, KS 67201

Box 51, Ltd.
Municipal Airport
Route 1, Box 102
Denton, TX 76201

Christen Industries
P.O. Box 547
Afton, WY 83110

British Aerospace, Inc.
P.O. Box 17414
Dulles Int'l Airport
Washington, DC 20041-0414

Christen Industries, Inc.
Aircraft Manufacturing Division
P.O. Box 547
Afton, WY 83110

Burkhart-Grob of America
1070 Navajo Drive
Bluffton Airport Complex
Bluffton, OH 45817

De Havilland Aircraft of Canada
Garratt Boulevard
Downsview, Ontario M3K 1Y5
CANADA

Bushby Aircraft, Incorporated
647 Route 52
Mineola, IL 60447

Denney Aerocraft Company
6140 Morris Hill Lane
Boise, ID 83704

Cameron Balloons, U.S.
41 Enterprise Drive
Ann Arbor, MI 48103

DeVore Aviation Corporation
6104B Kircher Boulevard, NF.
Albuquerque, NM 87109

Canadair
274 Riverside Avenue
Westport, CT 06880
CANADA

Diehl Aero-Nautical
1855 North Elm
Jenks, OK 74037

CASA Aircraft USA, Inc.
1215 Jefferson Davis Highway
Suite 404
Arlington, VA 22202

Dornier Aviation-North America, Inc.
1213 Jefferson Davis Highway
#1001
Arlington, VA 22202

J. H. Industries, Limited
Graville House
131-135 Sloane Street
London SW1X9BB
ENGLAND

Eagle Balloons, Ltd.
Hanover Municipal Airport
Ashland, VA 23005

Earthstar Aircraft, Incorporated
Star Route
P.O. Box 313
Santa Margarita, CA 93453

Fipper Aircraft
1631 Ynez Road
Lompoc, CA 93290

Entire Aircraft Corporation
125 SW. 34 Street
Fort Lauderdale, FL 33315

Instar Helicopter Corporation
Two County Airport
P.O. Box 177
Marinette, MI 49858

Futuraire Aircraft Corporation
P.O. Box 12486
San Antonio, TX 78284

Falcon Jet Corporation
Teterboro Airport
Teterboro, NJ 07608

Foster Dillen Products, Incorporated
P.O. Box 124
South Webster, OH 45682

Fokker Aircraft USA, Inc.
1199 North Fairfax Street
Suite 500
Alexandria, VA 22314

Freedom Master Corporation
450 Hamlin Avenue
Satellite Beach, FL 32937

Galaxy Balloons, Inc.
820 Salisbury Road
Statesville, NC 28677

Gates Learjet Corporation
P.O. Box 11186
Tucson, AZ 85734

General Aviaiton
Manufacturers Association
1400 K Street, NW.
Suite 801
Washington, DC 20005

Glaser Dirks Sailplanes, Inc.
5847 Sharpe Road
Calistoga, CA 94515

Graham Thomson, Ltd.
P.O. Box 1175
Pacific Palisades, CA 90272

Gulfstream Aerospace Corporation
Wiley Post Airport
P.O. Box 22500
Oklahoma City, OK 73123

Head Balloons, Inc.
550 Echelon Road
Greenville, SC 29605

Bones Aviation Industries
P.O. Box 697
Frederick, OK 73542

Litecraft, Inc.
Route 4, Box 48
Vacherie, LA 70096

NAV Limited
445 West 10th Avenue
Evan, Box 2984
Milwaukee, WI 54903

One Aircraft and Arms
Germany, Inc.
115 Broadway
New York, NY 10007

One Park Manufacturing
11-52 Western Avenue
Stanford, CA 94660

S. Knowles Sport Aircraft, Incorporated
14 East Avenue
P.O. Unit G
Lancaster, CA 93535

Patt Company
Box 1 Delivery 3
P.O. Box 19
Canonsville, PA 19460

Param Aircraft
Laconia Airport Hangar 1
Laconia, NH 03246

Point Aero, Incorporated
102 Aviation Way
P.O. Box 728
Alturas, ID 83606

Right Miniature Aircraft
Building #14
La Grange Airport
La Grange, FL 33054

Lockheed Georgia Company
Technical Reports Department
Department 72-34, Zone 235
86 South Cobb Drive
Marietta, GA 30063

Loehle Aviation, Incorporated
Shipmans Creek Road
Wartrace, TN 37183

Mael Aircraft Corporation
Box 138
Portage, WI 53901

Maule Aircraft Corporation
Lake Maule
Route 5, Box 319
Moultrie, GA 31768

MBB Helicopter Corporation
900 Airport Road
P.O. Box 2349
West Chester, PA 19380

McDonnell Douglas Corporation
3855 Lakewood Boulevard
Long Beach, CA 90846

McDonnell Douglas Helicopter
Company
Centinela and Teale Streets
Culver City, CA 90230

Melex USA, Inc.
1200 Front Street
Suite 101
Raleigh, NC 27609

Mike Smith Aero
Box 430
Stanton County Airport
Johnson City, KS 67855

Osprey Aircraft
3741 El Ricon Way
Sacramento, CA 95825

Mooney Aircraft Corporation
P.O. Box 72
Kerrville, TX 78028-0072

Partenavia of America
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Morris Aviation, Ltd.
P.O. Box 710
Statesboro Airport
Statesboro, GA 30458

Pazmany Aircraft Corporation
P.O. Box 80051
San Diego, CA 92138

Mudry Aviation, Ltd.
Dutchess City Airport
Route 378
Wappingers Falls, NY 12590

PIK Pacific
1231 Second Street
Manhattan Beach, CA 90266

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Company, Incorporated
P.O. Box 1118
Independence, MO 64055

Piper Aircraft Corporation
Box 1328
Vero Beach, FL 32961

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Santa Paula, CA 93060

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Fredericksburg, NC 28739

Quad City Aircraft Corporation
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Nuvaco Aircraft
2475 East Euclid Place
Littleton, CO 80121

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Huntington Beach, CA 92649

OMAC, Inc.
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Albany, GA 31708

Rans Company
1104 East Highway 40 Bypass
Hays, KS 67601

Raven Industries, Inc.
421 West Eighteenth Street
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Sioux Falls, SD 57101

Shorts Brothers, USA, Inc.
2011 Crystal Drive
Suite 713
Arlington, VA 22202-3702

Robinson Helicopter Company
24747 Crenshaw Boulevard
Torrance, CA 90505

Sikorsky Aircraft
North Main Street
Stratford, CT 06601

Regerson Aircraft Corporation
2201 Alton Avenue
Irvine, CA 92714

Silhouette Aircraft Sales, Incorporated
848 East Santa Maria Street
Santa Paula, CA 93060

Rotec Engineering, Incorporated
P.O. Box 220
Duncanville, TX 75138

Skypower
Box 236
Tea, SD 57064

Rotorway Aircraft
7411 West Galveston
Chandler, AZ 85224

Sorrell Aviation, Limited
16525 Tilley Road, S.
Tenino, WA 98589

SAAB Aircraft of America, Inc.
200 Fairbrook Drive
Herndon, VA 22070

Spencer Amphibian Air Car, Incorporated
11019 Glenoaks Boulevard
Pacoima, CA 91331

Schleicher Sailplanes, Inc.
P.O. Box 118
Port Matilda, PA 16870

Squadron Aviation, Incorporated
P.O. Box 2376
Columbus, OH 43223

Schweizer Aircraft Corporation
P.O. Box 147
Elmira, NY 14902

Star-Lite Aircraft, Incorporated
2219 Orange Blossom
San Antonio, TX 78247

Sequoia Aircraft Corporation
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Stoddard-Hamilton Aircraft,
Incorporated
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Arlington, WA 98223

Stolp Starduster Corporation
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Riverside, CA 92509

War Aircraft Replica, Incorporated
348 South Eighth Street
Santa Paula, CA 93060

Swearingen Aircraft Corporation
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San Antonio, TX 78214

Weatherly Aviation Company
2304 San Felipe Road
Hollister, CA 95023

Taylorcraft Aviation Corporation
P.O. Box 947
828 First Bald Eagle Street
Lock Haven, PA 17745

Westland, Inc.
7135 Jefferson Davis Highway
Suite 805
Arlington, VA 22202

Teenie Company
P.O. Box 625
Chalidage, AZ 85228

White Lightning Aircraft Corporation
P.O. Drawer 40
Sheldon, SC 29941

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812 Salisbury Road
Statesville, NC 28677

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Nobleton, Ontario
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Box 320
Chatham, NY 12037-0320

Ultimate Aerobatics, Limited
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Van's Aircraft, Incorporated
P.O. Box 160
North Plains, OR 97133

Wag-Aero, Incorporated
P.O. Box 181
Lyons, WI 53148

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ASF-1 - Office of Aviation Safety

AST-1 - Office of Science & Advanced Technology

APM-1 - Program Engineer & Maintenance Service

AVS-1 - Associate Administrator for Aviation Standards

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